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Automation and Remote Control

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Contents

Automation and Remote Control Vol. 85, No. 5, 2024

Topical Issue

Introduction P. S. Shcherbakov	451
Boris Polyak: The List of Research Works	452
An Optimal Choice of Characteristic Polynomial Roots for Pole Placement Control Design V. A. Alexandrov	479
On Some Problems with Multivalued Mappings M. V. Balashov, K. Z. Biglov, and A. A. Tremba	491
Approximation-Based Approach to Adaptive Control of Linear Time-Varying Systems A. Glushchenko and K. Lastochkin	512
Investigation of Feasible and Marginal Operating Regimes of Electric Power Systems E. N. Gryazina and D. Y. Baluev	532
Iterative Methods with Self-Learning for Solving Nonlinear Equations Yu. S. Popkov	544

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TOPICAL ISSUE



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On February 3, 2023, an outstanding mathematician and a wonderful person, Boris Teodorovich Polyak passed away. For a long time he headed Laboratory 7 of the Institute of Control Sciences, RAS, and was a generator of bright scientific ideas for decades, so we decided to arrange a special issue of the journal Automation and Remote Control, dedicated to his memory. The articles in this collection are mostly authored by the members of our lab, and the publication of this issue is not devoted to the sad anniversary of the death of Boris Teodorovich, but to his birthday on May 4, 1935.

The range of scientific interests of Prof. Polyak is striking in its diversity, as can be seen from the list of research papers which he authored and which we present in our issue. It is also worth mentioning that, in addition to the breadth of interests of Boris Teodorovich, this bibliography list testifies to a large number of his co-authors, — he has always generously shared his ideas with both students and younger followers and older colleagues.

Of course, within the framework of one issue, it is impossible to cover all areas of research interest of Boris Teodorovich, but we tried to collect articles on the topics that interested him most in recent years. These include the optimization theory, which he loved since his youth, and the methods of the classical theory of automatic control, robustness and rejection of exogenous disturbances, linear matrix inequalities, superstability, applied problems of energy systems research, and the peak effect. Due to the limitations on the volume of one issue, some of the submitted articles were transferred to the 6th issue of the journal.

Next year we plan to publish another special issue dedicated to the 90th anniversary of Prof. Polyak; the circle of authors is expected to be much wider.

On behalf of all members of lab. 7 of the Instutute of Control Science, Editior of the issue, P.S. Shcherbakov ISSN 0005-1179 (print), ISSN 1608-3032 (online), Automation and Remote Control, 2024, Vol. 85, No. 5, pp. 452-478. © The Author(s), 2024 published by Trapeznikov Institute of Control Sciences, Russian Academy of Sciences, 2024. Russian Text © The Author(s), 2024, published in Avtomatika i Telemekhanika, 2024, No. 5, pp. 5-41.

TOPICAL ISSUE

Boris Polyak: The List of Research Works¹

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¹ Compiled by P.S. Shcherbakov, A.A. Tremba, and Ya.I. Kvinto. The texts of almost all *journal articles* (and other publications) can be found at https://sites.google.com/site/lab7polyak/ © A.A. Tremba.

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At the time of compiling this list, some scientometric indicators of Boris Polyak's publications on Scopus/Google Scholar were as follows: the Hirsch index, 33/64; the number of citations, over $9\,100/31\,600$ (with a constant growth rate since 2004 and an "exponential" one since 2015); the two most cited articles, [3.6] (over $1\,600/3\,300$ citations) and [3.67] (about $1\,100/2\,300$ citations); the number of coauthors, 81.

The compilers of this list are grateful to the readers for possible additions as well as indications of inaccuracies and simple mistakes. In our point of view, for experts in the corresponding fields of science, the list of Boris Polyak's research works well characterizes the epoch and reflects the popularity of various topics and the change of priorities over time. A complete and accurate bibliography will be published in a separate brochure. ISSN 0005-1179 (print), ISSN 1608-3032 (online), Automation and Remote Control, 2024, Vol. 85, No. 5, pp. 479-490. © The Author(s), 2024 published by Trapeznikov Institute of Control Sciences, Russian Academy of Sciences, 2024. Russian Text © The Author(s), 2024, published in Avtomatika i Telemekhanika, 2024, No. 5, pp. 42-57.

TOPICAL ISSUE

An Optimal Choice of Characteristic Polynomial Roots for Pole Placement Control Design

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Abstract—The problem of finding the arrangement of closed-loop control system poles that minimizes an objective function is considered. The system optimality criterion is the value of the H_{∞} norm of the frequency transfer function relative to the disturbance with constraints imposed on the system pole placement and the values of the H_{∞} norm of the sensitivity function and the transfer function from measurement noise to control. An optimization problem is formulated as follows: the vector of variables consists of the characteristic polynomial roots of the closed loop system with the admissible values restricted to a given pole placement region; in addition to the optimality criterion, the objective function includes penalty elements for other constraints. It is proposed to use a logarithmic scale for the moduli of the characteristic polynomial roots as elements of the vector of variables. The multi-extremality problem of the objective function is solved using the multiple start procedure. A coordinate descent modification with a pair of coordinates varied simultaneously is used for search.

Keywords: control design, transfer function, pole placement, optimization, robust system

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1. INTRODUCTION

Rejection of an unmeasurable disturbance is one of the main tasks of control design [1]. On the other hand, the resulting system must satisfy robustness conditions since the plant model used for control design is inaccurate. For linear systems, first of all, the requirements for stability margins must be met [2]. These requirements can be specified as the minimum acceptable stability margins radius [3] or limiting the value of the sensitivity function [4, 5]. The H_{∞} norm of the measurement noise sensitivity function can serve as a measure of robustness to unmodeled dynamics [5, 6].

Many control design techniques lead to an optimization problem. For example, the methods of H_{∞} optimization [7] and invariant ellipsoids [1] reduce to an optimization procedure for solving a system of linear matrix inequalities. If the variables are the coefficients of a fixed-structure controller, the optimization problem may become non-convex and multi-extremal [8, 9]. The successful results of solving such problems allowed developing similar approaches for tuning PID controllers widely used in practice [10, 11].

For a linear single-input single-output (SISO) system, the following idea of optimization of the closed-loop system pole placement was proposed in [12]: the controller coefficients are found via the standard pole placement procedure, and the roots of the desired characteristic polynomial of the closed loop system are searched using an optimization procedure for specified quality criteria and constraints. The standard global optimization procedure from the MATLAB Global Optimization Toolbox [13] was used in [12]. The value of the H_{∞} norm of the transfer function relative to the disturbance was chosen as a quality criterion under given constraints on the values of the H_{∞} norms

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of the sensitivity function and the transfer function from measurement noise to control. In addition, constraints were imposed on the system pole placement.

This article is devoted to developing an optimization procedure for finding an optimal closed-loop system pole placement that minimizes a given objective function subject to specified constraints; in the corresponding optimization problem, the vector of variables consists of the characteristic polynomial roots of the closed loop system.

2. PROBLEM STATEMENT

Consider a linear SISO system whose structure is presented in Fig. 1. Let the plant be described by the transfer function

$$P(s) = \frac{b(s)}{a(s)} = \frac{b_{n-1}s^{n-1} + \dots + b_0}{s^n + a_{n-1}s^{n-1} + \dots + a_0},$$
(1)

where s is the Laplace transform variable; the coefficients $a_i, b_i \in \mathbb{R}$ (i = 0, ..., n - 1) have known values, and at least one of the coefficients b_i is nonzero; the polynomials a(s) and b(s) are coprime. The frequency response function is obtained for $s = j\omega$, where $\omega \in [0, \infty)$. By assumption, as frequency response functions are used, all system signals (including the unmeasured exogenous disturbance) are integrable and satisfy the restrictions for applying the Fourier transform [2]:

$$\int_{-\infty}^{+\infty} |f(t)| dt < \infty.$$

Suppose that the controller's transfer function has the form

$$C(s) = \frac{d(s)}{c(s)} = \frac{d_{n-1}s^{n-1} + \dots + d_0}{c_{n-1}s^{n-1} + \dots + c_0},$$
(2)

where the controller order (n-1) is determined by the order of the plant model (1). A higher-order controller, which can be constructed, e.g., by adding an integral component to the controller, is not considered here. A lower-order controller cannot be constructed by the pole placement technique; see the explanation below.

According to the pole placement method [14, 15], the polynomials c(s) and d(s) of the controller (2) can be obtained by solving the equation

$$a(s)c(s) + b(s)d(s) = \delta(s), \tag{3}$$

where the left-hand side is the characteristic polynomial of system (1), (2) in which a(s) and b(s) are the known polynomials of the plant's transfer function, and $\delta(s)$ is a given desired characteristic polynomial. As is known [14], there exists a unique solution of this equation under the condition $\deg d(s) < \deg a(s)$ or $\deg c(s) < \deg b(s)$. In addition, under the condition $\deg \delta(s) \ge 2 \deg a(s) - 1$,



Fig. 1. Closed loop system: y—measured output, ν —measurement noise, r—reference signal, e—control error, u—control, and f—disturbance.

the causality of control is satisfied: $\deg d(s) \leq \deg c(s)$. Then, by choosing the desired polynomial $\delta(s)$ of degree $\deg \delta(s) = 2 \deg a(s) - 1$, we obtain the solution (2) for which the conditions $\deg d(s) \leq \deg c(s)$ and $\deg d(s) < \deg a(s)$ hold. In this case, equation (3) can be solved by compiling a system of 2n linear algebraic equations with 2n unknowns when equating the coefficients of the left- and right-hand sides of equation (3) at the equal powers of s:

$$\begin{bmatrix} c_{n-1} \\ \cdots \\ c_0 \\ d_{n-1} \\ \cdots \\ d_0 \end{bmatrix} = W^{-1} \begin{bmatrix} \delta_{2n-1} \\ \cdots \\ \delta_0 \end{bmatrix},$$
(4)

where $W \in \mathbb{R}^{2n \times 2n}$ is a matrix obtained from the coefficients $a_i, b_i \ (i = 0, \dots, n-1)$.

Thus, for any plant (1), one can find a controller of the form (2) ensuring any given characteristic polynomial $\delta(s)$ of degree (2n-1) for the closed loop system. Note that for an unstable plant of order n, there may not exist a controller of order below (n-1) ensuring at least the stability of the system. Therefore, we consider a controller of order (n-1) to ensure not only stability but also other system properties of the system by choosing an appropriate desired characteristic polynomial.

The characteristic polynomial can be represented as

$$\delta(s) = \prod_{i=1}^{n_r} (s + \lambda_i) \prod_{k=1}^{n_c} (s^2 + 2\zeta_k \breve{\omega}_k s + \breve{\omega}_k^2), \tag{5}$$

where $n_r = 2n - 2n_c - 1$ is the number of real roots of the polynomial $\delta(s)$ and n_c is the number of complex conjugate pairs of the roots; the values $\lambda_i, \breve{\omega}_k \in \mathbb{R}$ and $\zeta_k \in [0, 1]$ determine the closedloop pole placement and the coefficients $\delta_0, \ldots, \delta_{2n-2}$ in (4) while $\delta_{2n-1} = 1$. Let $\breve{\omega}_k$ denote the natural frequencies of the system since the notation ω is used for the frequency variable in transfer functions.

In addition to the standard constraints $\lambda_i > 0$, $\breve{\omega}_k > 0$, and $0 < \zeta_k \leq 1$, which ensure the stability of the closed loop system, it is possible to specify the supplementary ones

$$0 < \lambda_{\min} \leqslant \lambda_i \leqslant \lambda_{\max}, \quad 0 < \breve{\omega}_{\min} \leqslant \breve{\omega}_k \leqslant \breve{\omega}_{\max}, \quad 0 < \zeta_{\min} \leqslant \zeta_k \leqslant 1$$
(6)

to obtain the desired speed and damping rate of the system and limit the high-frequency components.

Similar to [12], the value of H_{∞} norm of the frequency response function relative to the disturbance is taken as the system quality criterion:

$$\|G_{yf}(j\omega)\|_{\infty} = \sup_{\omega} \left| \frac{b(j\omega)c(j\omega)}{\delta(j\omega)} \right|.$$
(7)

Moreover, the following constraints must be satisfied:

— for the H_{∞} norm of the sensitivity function, the inequality

$$\|S(j\omega)\|_{\infty} = \sup_{\omega} \left| \frac{a(j\omega)c(j\omega)}{\delta(j\omega)} \right| \leqslant S_{\max}$$
(8)

to ensure the required stability margins;

— for the H_{∞} norm of the frequency response function relative to the noise, the inequality

$$\|G_{u\nu}(j\omega)\|_{\infty} = \sup_{\omega} \left|\frac{a(j\omega)d(j\omega)}{\delta(j\omega)}\right| \leqslant N_{\max}$$
(9)

to ensure the robustness of the system in the presence of unmodeled dynamics by limiting the controller gain [5, 6].

Thus, the problem is to find a controller of the form (2) that minimizes the exogenous disturbance effect on the the plant (1) in terms of the norm (7) subject to the constraints (6), (8), and (9) under given values a_i, b_i $(i = 0, ..., n - 1), \lambda_{\min}, \lambda_{\max}, \breve{\omega}_{\min}, \breve{\omega}_{\max}, \zeta_{\min}, S_{\max}$, and N_{\max} . It can be formulated as an optimization problem.

Problem 1. Find

$$\min_{x \in Q} \|G_{yf}(j\omega, x)\|_{\infty}$$

subject to

$$\|S(j\omega, x)\|_{\infty} \leqslant S_{\max},$$

$$\|G_{u\nu}(j\omega, x)\|_{\infty} \leqslant N_{\max},$$
(10)

where S_{max} and N_{max} are given values. The vector of variables $x \in \mathbb{R}^{2n-1}$ has the form

$$x = [\lambda_1, \dots, \lambda_{n_r}, \breve{\omega}_1, \dots, \breve{\omega}_{n_c}, \zeta_1, \dots, \zeta_{n_c}], \tag{11}$$

where n_r and n_c are given values such that $0 \leq n_c \leq n-1$, $n_r = 2n - 2n_c - 1$, and n is a known order of the plant (1). The admissible region Q is determined by inequalities (6) with the given parameters $\lambda_{\min}, \lambda_{\max}, \check{\omega}_{\min}, \check{\omega}_{\max}$, and ζ_{\min} . In accordance with (7)–(9), the frequency response functions $G_{yf}(j\omega, x), S(j\omega, x)$, and $G_{u\nu}(j\omega, x)$ are constructed from the given polynomials $a(j\omega)$ and $b(j\omega)$ of the plant (1), the polynomial $\delta(j\omega)$ determined for the vector (11) by formula (5), and the controller polynomials $c(j\omega)$ and $d(j\omega)$ whose coefficients are found by solving system (4).

Note that the constraints (6), (8), and (9) may be not satisfied simultaneously; in this case, the set of admissible values will be empty. This issue is not considered here: the constraints are assumed to be consistent. For a particular problem, an iterative process can be carried out in practice to find acceptable values of the constraints for reaching an acceptable value of the objective function.

3. SEARCH FOR THE OPTIMAL ROOTS OF THE CHARACTERISTIC POLYNOMIAL

3.1. Objective Function with Penalties

We use the penalty function method to satisfy the constraints. For the value $||G(j\omega, x)||_{\infty}$, the penalty function $\tilde{G}(x)$ is given by

$$\tilde{G}(x) = \begin{cases} 0 \text{ if } \|G(j\omega, x)\|_{\infty} \leq G_{\max} \\ \ln \frac{\|G(j\omega, x)\|_{\infty}}{G_{\max}} & \text{if } \|G(j\omega, x)\|_{\infty} > G_{\max}. \end{cases}$$
(12)

In this case, the objective function takes the form

$$f(x) = \|G_{yf}(j\omega, x)\|_{\infty} + \mu_1 S(x) + \mu_2 G_{u\nu}(x),$$
(13)

where $\mu_1 > 0$ and $\mu_2 > 0$ are weight coefficients, and S(x) and $G_{u\nu}(x)$ are the penalty functions obtained using (12) for the constraints (10). Note that due to (12), the objective function (13) is non-differentiable at the points where $||S(j\omega, x)||_{\infty} = S_{\max}$ or $||G_{u\nu}(j\omega, x)||_{\infty} = N_{\max}$. Moreover, the functions (7)–(9) may be non-convex and multi-extremal, and their gradients are not written in explicit form.
3.2. Scaling of the Variables

The logarithmic scale is often used to analyze dynamic systems in the frequency domain [2]. Note that the elements λ_i and $\breve{\omega}_k$ of the vector of variables (11) are the natural frequencies of the system. We convert them to a logarithmic scale, thus assigning a greater weight to changes in the roots with a modulus close to zero (slow system dynamics) compared to changes in those with a large modulus (fast system dynamics):

$$\tilde{x} = [\lg \lambda_1, \dots, \lg \lambda_{n_r}, \lg \breve{\omega}_1, \dots, \lg \breve{\omega}_{n_c}, \zeta_1, \dots, \zeta_{n_c}] = [\tilde{\lambda}_1, \dots, \tilde{\lambda}_{n_r}, \tilde{\omega}_1, \dots, \tilde{\omega}_{n_c}, \zeta_1, \dots, \zeta_{n_c}],$$
(14)

where λ_i and $\tilde{\omega}_i$ are the common logarithms of the variables λ_i and $\tilde{\omega}_i$, respectively. In this case, the constraints (6) take the form

$$0 < \lg \lambda_{\min} \leqslant \lambda_i \leqslant \lg \lambda_{\max},$$

$$0 < \lg \breve{\omega}_{\min} \leqslant \tilde{\omega}_k \leqslant \lg \breve{\omega}_{\max},$$

$$0 < \zeta_{\min} \leqslant \zeta_k \leqslant 1.$$
(15)

To calculate the objective function, the values of the variables must be rescaled to (11) by raising to the tenth power: $\lambda_i = 10^{\tilde{\lambda}_i}, i = 1, \ldots, n_r$, and $\check{\omega}_i = 10^{\tilde{\omega}_i}, i = 1, \ldots, n_c$. The notations without the subscripts, $\tilde{\lambda}, \tilde{\omega}$, and ζ , will be used for the corresponding groups in the vector of variables (14):

$$\begin{split} \tilde{\lambda} &= [\tilde{\lambda}_1, \dots, \tilde{\lambda}_{n_r}], \\ \tilde{\omega} &= [\tilde{\omega}_1, \dots, \tilde{\omega}_{n_c}], \\ \zeta &= [\zeta_1, \dots, \zeta_{n_c}]. \end{split}$$

Accordingly, the vector (14) will be represented as $\tilde{x} = [\lambda, \tilde{\omega}, \zeta]$.

The dynamics with frequencies exceeding manyfold the minimum natural frequency of the control plant are often neglected during system design. Therefore, the difference between the common logarithms of the admissible values of the moduli of the characteristic polynomial roots usually is not greater than 5. For example, when considering a system with slow dynamics and $\lambda_{\min} = 0.001$ and $\lambda_{\max} = 1$, we obtain $\lg \lambda_{\min} = -3$ and $\lg \lambda_{\max} = 0$; for a system with fast dynamics, $\lg \lambda_{\min} = 2$ and $\lg \lambda_{\max} = 6$ under the same or similar values for $\lg \check{\omega}_{\min}$ and $\lg \check{\omega}_{\max}$. Then the choice of the minimum step for the groups of variables $\tilde{\lambda}$ and $\tilde{\omega}$ is obvious. It follows from practical considerations that a step from 0.0001 to 0.01 will be quite small under such scales. This step is also reasonable for the group ζ , whose elements belong to the range $[\zeta_{\min}, 1]$.

3.3. Multiple Start

Multiple start is a standard approach to settling the multi-extremality problem of the objective function (13): the search procedure is executed from different initial points. For the problem under consideration, the initial values can be chosen, e.g., using the following rule:

- Choose the number of alternatives n_1, n_2 , and n_3 for the groups of variables $\lambda, \tilde{\omega}$, and ζ , respectively.
- For the groups λ and $\tilde{\omega}$, create alternatives in which the first elements of the groups are uniformly distributed in the admissible range and the remaining elements are uniformly distributed in the

range $[\lambda_1, \lg \lambda_{\max}]$ or $[\tilde{\omega}_1, \lg \tilde{\omega}_{\max}]$, respectively:

$$\tilde{\lambda}_{1}^{(\ell)} = \lg \lambda_{\min} + \ell \frac{\lg \lambda_{\max} - \lg \lambda_{\min}}{n_{1} + 1}, \ \ell = 1, \dots, n_{1},$$

$$\tilde{\lambda}_{i}^{(\ell)} = \tilde{\lambda}_{1}^{(\ell)} + (i - 1) \frac{\lg \lambda_{\max} - \tilde{\lambda}_{1}^{(\ell)}}{n_{r}}, \ i = 2, \dots, n_{r},$$

$$\tilde{\omega}_{1}^{(\ell)} = \lg \breve{\omega}_{\min} + \ell \frac{\lg \breve{\omega}_{\max} - \lg \breve{\omega}_{\min}}{n_{2} + 1}, \ \ell = 1, \dots, n_{2},$$

$$\tilde{\omega}_{i}^{(\ell)} = \tilde{\omega}_{1}^{(\ell)} + (i - 1) \frac{\lg \breve{\omega}_{\max} - \tilde{\omega}_{1}^{(\ell)}}{n_{c}}, \ i = 2, \dots, n_{c}.$$
(16)

— Use the same values for all elements of the group ζ :

$$\zeta_i^{(\ell)} = \begin{cases} \frac{1-\zeta_{\min}}{2} & \text{if } n_3 = 1\\ \zeta_{\min} + (\ell-1)\frac{1-\zeta_{\min}}{n_3 - 1} & \text{if } n_3 > 1, \end{cases} \qquad i = 1, \dots, n_c, \ \ell = 1, \dots, n_3. \tag{17}$$

— Create the set of $n_1 \cdot n_2 \cdot n_3$ initial points by combining all alternatives for each group.

For example, 32 initial points will be obtained if $n_1 = 4, n_2 = 4$, and $n_3 = 2$.

When building another grid of the initial values, one should keep in mind the following: the rearrangement of any elements within the groups $\tilde{\lambda}$ and $\tilde{\omega}$ makes no sense because, due to (5), the resulting polynomial $\delta(s)$ will be the same regardless of the order of the elements in the group.

3.4. Search Method

The objective function (13) is generally non-convex, multi-extremal, and non-differentiable at some points; therefore, standard search methods will not necessarily find a global minimum. For the problem under consideration, we use a combined method in which coordinate descent is applied for the group of variables ζ whereas the groups $\tilde{\lambda}$ and $\tilde{\omega}$ are merged to execute the search procedure by the pairs of coordinates. The dimension of the vector $[\tilde{\lambda}, \tilde{\omega}]$ equals $n_a = n_r + n_c$, and $n_a!/(2(n_a - 2)!)$ pairs can be made from the elements of this vector. For $n_a = 10$, we have 45 pairs, which is computationally feasible. For most practical 1D problems, this restriction will be satisfied; for higher-dimension problems, however, some pairs should be discarded. For example, only neighbor elements can be combined into pairs, which gives $(n_a - 1)$ pairs; alternatively, pairs can be formed separately for the groups $\tilde{\lambda}$ and $\tilde{\omega}$.

We determine the next point (k+1) after varying a pair of elements i, j $(i = 1, ..., n_a - 1, j = i + 1, ..., n_a)$ as follows:

$$\tilde{x}_{k+1} = \arg\min_{\alpha,\beta} f(\tilde{x}_k + \alpha e_i + \beta e_j), \tag{18}$$

where e_i and e_j are the vectors with ones for elements *i* and *j*, respectively, and zeros for all other elements; α and β are values from some set of variations, e.g.,

$$\alpha, \beta \in \{0, 0.001, -0.001, 0.01, -0.01\}.$$
 (19)

If the result of (18) is $\alpha = \beta = 0$, then a new point has not been obtained. If a new record value of the objective function is reached, then the 1D search procedure can be executed for the corresponding values α and β :

$$\tilde{x}_{k+1} = \arg\min_{\gamma} f(\tilde{x}_k + \gamma \alpha e_i + \gamma \beta e_j), \tag{20}$$

where, e.g., $\gamma \in \{0, 10\}$.

Fixed steps are used due to the nonconvexity of the objective function: finding an optimal step in a given direction may be a computationally difficult task.

When varying the elements of the groups $\tilde{\lambda}$ and $\tilde{\omega}$, we take into account that the objective function is independent of the rearrangement of these elements. Therefore, it is possible to fix an order of elements $\tilde{\lambda}_1 \leq \tilde{\lambda}_2 \leq \ldots \leq \tilde{\lambda}_{n_r}$, $\tilde{\omega}_1 \leq \tilde{\omega}_2 \leq \ldots \leq \tilde{\omega}_{n_c}$ and, in addition to the bounds (15), use neighbor elements as bounds as well. For example, in the case $n_r > 2$,

$$\lambda_{1} \in [\lg \lambda_{\min}, \lambda_{2}],$$

$$\tilde{\lambda}_{i} \in [\tilde{\lambda}_{i-1}, \tilde{\lambda}_{i+1}], \ 1 < i < n_{r},$$

$$\tilde{\lambda}_{n_{r}} \in [\tilde{\lambda}_{n_{r}-1}, \lg \lambda_{\max}].$$
(21)

After the search procedure (18) for all pairs $(i = 1, ..., n_a - 1, j = i + 1, ..., n_a)$, we execute coordinate descent for the group ζ :

$$\tilde{x}_{k+1} = \arg\min_{\eta} f(\tilde{x}_k + \eta e_i), \ i = 1, \dots, n_c,$$
(22)

where η is the set of fixed steps and e_i is the vector with one for element $(i + n_r + n_c)$ and zeros for the other elements. For example, the set of steps can be

$$\eta \in \{0.001, -0.001, 0.01, -0.01, 0.05, -0.05\}.$$
(23)

The elements of the group ζ are varied within the specified bounds: $\zeta_i \in [\zeta_{\min}, 1]$.

Thus, Problem 1 is solved using the following algorithm for $n_a > 1$.

Algorithm 1.

1. Choose the penalty weight coefficients μ_1 and μ_2 for the objective function (13) and set the search threshold ε .

2. Generate a grid of initial points as described in subsection 3.3 and take the first initial point.

3. Calculate the value of the objective function at the initial point, $f_{\min}^{(\ell)}$.

4. Take a pair of elements from the groups of variables λ and $\tilde{\omega}$.

5. Execute (18) through the exhaustive search procedure over the set (19).

6. If a new record value of the objective function is obtained, execute (20) in the obtained direction and go to the new point.

7. Take the next pair of elements from the groups of variables λ and $\tilde{\omega}$ and revert to Step 5. If the exhaustive search procedure for the pairs is completed, proceed to Step 8.

8. If $n_c > 0$, take an element of the group ζ . Otherwise, proceed to Step 11.

9. Execute (22) through the exhaustive search procedure over the set (23).

10. Take the next element from the group ζ and revert to Step 9. If the exhaustive search procedure within the group ζ is completed, proceed to Step 11.

11. If the record value of the objective function \hat{f} yielded by Steps 4–10 is less than $f_{\min}^{(\ell)} - \varepsilon$, replace the value $f_{\min}^{(\ell)}$ with \hat{f} and revert to Step 4 with the corresponding new point. Otherwise, remember the objective function value $\min(f_{\min}^{(\ell)}, \hat{f})$ and the corresponding point \tilde{x} , take the next initial point, and revert to Step 3. If the search procedure for all initial points obtained in Step 2 is completed, proceed to Step 12.

12. Find the minimum among the objective function values obtained for all initial points and the corresponding point \tilde{x} . Complete the search procedure.

Additional search stages can be embedded in this algorithm if the objective function value does not decrease in Step 11: 1) increase the weight coefficients μ_1 and μ_2 and continue the search procedure from the resulting point; 2) continue the search procedure with smaller values of the set of variations (19) for α and β .

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AUTOMATION AND REMOTE CONTROL Vol. 85 No. 5 2024
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ALEXANDROV

4. EXAMPLES

4.1. Underwater Vehicle Position Control

The transfer functions for local coordinate system positioning were identified in [16]. In this section, we consider control design for the coordinate z with the identified transfer function

$$P_z(s) = \frac{0.018}{s(0.98s+1)}.$$
(24)

The two-degree-of-freedom (2DOF) PID controller presented in [16] allows setting a desired transfer function of the closed loop system. For this example, we take the desired transfer function

$$P_m(s) = \frac{1}{(0.98s+1)(0.5s+1)}.$$
(25)

The denominator of the transfer function (25) must be included in the desired characteristic polynomial of the closed loop system when designing a 2DOF controller. Then there are only two roots left for variation. Assume that they form a complex conjugate pair of roots of the characteristic polynomial. In this case, the controller coefficients

$$C(s) = \frac{d_2 s^2 + d_1 s + d_0}{s(c_1 s + c_0)}$$
(26)

are obtained from the equation

 $s^{2}(0.98s+1)(c_{1}s+c_{0})+0.018(d_{2}s^{2}+d_{1}s+d_{0})=(0.98s+1)(0.5s+1)(s^{2}+2\zeta\breve{\omega}+\breve{\omega}^{2}).$

This example illustrates the search procedure for the variables ζ and $\check{\omega}$. Since $n_a = 1$ here, we use coordinate descent instead of Algorithm 1.

Let the following bounds be specified:

$$\breve{\omega}_{\min} = 0.6, \ \breve{\omega}_{\max} = 20, \ \zeta_{\min} = 0.8, \ S_{\max} = 1.7, \ N_{\max} = 150.$$
(27)

Weight coefficients should be assigned for the penalty functions of the objective function (13). These coefficients are chosen so that the constraints have priority over disturbance rejection. Note that the penalty functions are included in (13) as the ratio of the H_{∞} norm to its admissible



Fig. 2. Coordinate descent: $\tilde{x} = [\tilde{\omega}, \zeta]$.

maximum value whereas the H_{∞} norm of the frequency response function relative to the disturbance is used in absolute units. Therefore, to choose the weight coefficients, it is necessary to estimate the value $\|G_{yf}(j\omega)\|_{\infty}$. For example, for the minimum values from the admissible region $\breve{\omega} = 0.6$, $\zeta = 0.8$, we obtain $\|G_{yf}(j\omega)\|_{\infty} = 0.0239$. Then the values $\mu_1 = 1$ and $\mu_2 = 0.1$ can be taken. The set of steps (23) is used for both variables.

Figure 2 shows the surface of the objective function on a grid with steps of 0.02 for $\tilde{\omega}$ and 0.01 for ζ within the given constraints. Also, this figure presents the objective function values in each step of the coordinate descent procedure with the initial point

$$\tilde{x}_0 = \left[\frac{\lg \breve{\omega}_{\max} + \lg \breve{\omega}_{\min}}{2}, \frac{1 + \zeta_{\min}}{2}\right] = [0.5396, 0.9].$$

The minimum point is $\breve{\omega} = 0.6928, \zeta = 0.821$, and the corresponding values are

$$||S(j\omega)||_{\infty} = 1.27, ||G_{u\nu}(j\omega)||_{\infty} = 149.97, ||G_{yf}(j\omega)||_{\infty} = 0.0206.$$

4.2. Controller for a Two-Mass System

Consider the benchmark problem presented in [17], i.e., a robust control design for two trolleys joined by a spring. For this problem, the pole placement optimization method was used to build a controller satisfying the speed and robustness requirements of the system [12]. Note that the standard global optimization procedure from the MATLAB Global Optimization Toolbox [13] was applied therein to find the optimal roots of the characteristic polynomial. In this subsection, we use Algorithm 1 to solve the same problem.

Let the transfer function relative to control be

$$P(s) = \frac{1}{s^2(s^2 + 2)}.$$
(28)

In this plant, control and disturbance are applied at different points, and the open-loop transfer function relative to the disturbance is known:

$$P_f(s) = \frac{s^2 + 1}{s^2(s^2 + 2)}.$$
(29)

In this case, the H_{∞} norm of the closed-loop frequency transfer function relative to the disturbance differs from (7) and is calculated as

$$\|G_{yf}(j\omega)\|_{\infty} = \sup_{\omega} \left| \frac{b_f(j\omega)c(j\omega)}{\delta(j\omega)} \right|,\tag{30}$$

where $b_f(j\omega)$ is the numerator polynomial of the transfer function (29).

Similar to [12], we design a controller of the form (2) with n = 4 under the following bounds and constraints:

$$\lambda_{\min} = \breve{\omega}_{\min} = 0.1, \ \lambda_{\max} = \breve{\omega}_{\max} = 100, \ \zeta_{\min} = 0.7, \ S_{\max} = 1.665, \ N_{\max} = 100.$$
 (31)

We choose the desired structure of the characteristic polynomial (5) with $n_r = 1$ and $n_c = 3$ and the weight coefficients $\mu_1 = \mu_2 = 100$ for the penalty functions in (13). Let the threshold for varying the objective function be $\varepsilon = 10^{-6}$. We form twenty-four initial points for multiple start by choosing $n_1 = 4$, $n_2 = 3$, and $n_3 = 2$ and using (16) for the groups $\tilde{\lambda}$ and $\tilde{\omega}$ as well as the following alternatives for the group $\zeta : 1$) all elements equal ζ_{\min} ; 2) all elements equal one.

ALEXANDROV



Fig. 3. The values of the objective function f(x) at each iteration of the search algorithm.



Fig. 4. The values of the objective function $f(\tilde{\lambda}_1, \tilde{\omega}_1)$.

The resulting minimum point of the objective function (13) is

$$x_{\min} = [0.3417, 1.4138, 1.4145, 3.6593, 0.701, 0.700, 0.700], \tag{32}$$

for which

$$||S(j\omega)||_{\infty} = 1.665, \quad ||G_{u\nu}(j\omega)||_{\infty} = 99.96, \quad ||G_{yf}(j\omega)||_{\infty} = 5.296.$$
(33)

The minimum was found in twenty iterations from an initial point. Figure 3 shows the graph of the record values of the objective function. Other six points of multiple start yielded $||G_{yf}(j\omega)||_{\infty} < 6$ under the valid constraints. The remaining initial points led to local minima with the invalid constraint $||S(j\omega)||_{\infty} \leq S_{\max}$ or a higher value of $||G_{yf}(j\omega)||_{\infty}$. Only two of the twenty-four initial

points of multiple start resulted in the same local minimum; in the rest cases, the search procedure was completed at different points.

Figure 4 shows the surface of the objective function calculated for the vector \tilde{x} with only the first two elements being varied on a grid (and the rest equaling the obtained values (32)) and search alternatives for these two elements from the initial points [0.5, 0.5] and [-1, 0.5]. Obviously, the search procedure converged to different local minima with values of the objective function equal to 19.8 and 5.3, respectively. In other words, the objective function in this example has a complicated ravine surface even in the simplified case with two variables.

The same example with the same constraints was solved by several methods in [12]. The controller with $||G_{yf}(j\omega)||_{\infty} = 5.301$, the result almost coinciding with (33), was obtained using systume, the fixed-structure control system tuning procedure [18] of the MATLAB Robust Control Toolbox. The solution by the pole placement optimization method using the standard global optimization procedure was implemented in [12]; the resulting controller rejects the disturbance slightly worse, ensuring the value $||G_{yf}(j\omega)||_{\infty} = 6.64$.

Thus, the search algorithm proposed in this article found a better solution than the standard global optimization procedure. The solution obtained by **systune** is practically not improved, which suggests its global minimum character.

5. CONCLUSIONS

The control design problem using the pole placement method has been considered, and an algorithm has been developed to find the desired poles based on the specified system quality criteria and constraints. The value of the H_{∞} norm of the frequency transfer function relative to the disturbance has been selected as the quality criterion of the system, and the maximum admissible values of the H_{∞} norms of the sensitivity function and the frequency transfer function relative to the measurement noise have been set as the constraints. The resulting search algorithm can be used for other criteria and constraints. In this case, only the penalty components (12) in the objective function (13) will be changed. Note that in the example of subsection 4.1, the controller structure differs from (2) since an integral component has been added to the controller. Thus, the scope of application of the developed approach is not restricted to systems with the controller (2): it covers all controller structures that can be obtained by the pole placement method. Also, for the sake of simplicity, an exogenous disturbance has been applied along with the control action in the system structure. Indeed, the real transfer function relative to the disturbance is often unknown; in this case, such a simplification of the system structure still allows considering the effect of the disturbance in the system. If the plant's transfer function relative to the disturbance is known (see the example of subsection 4.2), it should be used when forming the transfer function of the closed loop system relative to the disturbance.

The advantages of the proposed search method are due to considering the properties of the characteristic polynomial roots. The logarithmic scale taken for the moduli of the characteristic polynomial roots provides the following benefits. First, it serves to reasonably choose the increment of the variables in the search procedure. Second, it allows one to form a limited set of initial points for the multiple start procedure. The search algorithm with a pair of simultaneously varied elements finds the minimum for an objective function with a complicated surface. Thus, the known features of the vector of variables in the problem under consideration have been utilized to develop an effective constrained minimization algorithm for a non-convex multi-extremal objective function.

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ALEXANDROV

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TOPICAL ISSUE

On Some Problems with Multivalued Mappings

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Abstract—We consider some problems with a set-valued mapping, which can be reduced to minimization of a homogeneous Lipschitz function on the unit sphere. Latter problem can be solved in some cases with a first order algorithm—the gradient projection method. As one of the examples, the case when set-valued mapping is the reachable set of a linear autonomous controlled system is considered. In several settings, the linear convergence is proven. The methods used in proofs follow those introduced by B.T. Polyak for the case where Lezanski–Polyak–Lojasiewicz condition holds. Unlike algorithms that use approximation of the reachable set, the proposed algorithms depend far less on dimension and other parameters of the problem. Efficient error estimation is possible. Numerical experiments confirm the effectiveness of the considered approach. This approach can also be applied to various set-theoretical problems with general set-valued mappings.

Keywords: gradient projection method, set-valued integral, strong convexity, supporting set, Lipschitz condition, nonsmooth analysis

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1. INTRODUCTION

Let \mathbb{R}^n be a real Euclidean space with the inner product (\cdot, \cdot) and norm $\|\cdot\| = \sqrt{(\cdot, \cdot)}$. Define the ball $\mathcal{B}_r(a) = \{x \in \mathbb{R}^n : \|x - a\| \leq r\}, (a \in \mathbb{R}^n, r > 0)$ and the unit sphere $\mathcal{S}_1 = \partial \mathcal{B}_1(0)$. Denote by int \mathcal{N} and $\partial \mathcal{N}$ the interior and the boundary of a set $\mathcal{N} \subset \mathbb{R}^n$, respectively. Recall that the supporting function for a closed convex set $\mathcal{N} \subset \mathbb{R}^n$ and vector $p \in \mathbb{R}^n$ is $s(p, \mathcal{N}) = \sup_{x \in \mathcal{N}} (p, x)$ and the supporting subset is $\mathcal{N}(p) = \{x \in \mathcal{N} : (p, x) = s(p, \mathcal{N})\}$. The set $\mathcal{N}(p)$ is called the supporting element if it is a singleton. For a convex compact set \mathcal{N} the set $\mathcal{N}(p)$ is the subdifferential (in the sense of convex analysis) of the supporting function $s(p, \mathcal{N})$ at the point p. Let $P_{\mathcal{N}}x$ be the metric projection of a point $x \in \mathbb{R}^n$ onto a closed convex set \mathcal{N} .

Let $\mathcal{N} \subset \mathbb{R}^n \setminus \{0\}$ be a convex compact set and $f(p) = s(p, \mathcal{N})$. Consider the problem

$$\min_{\|p\|=1} f(p) = J.$$
(1)

It is obvious that the solution of problem (1) is a unit vector p_0 such that $p_0 = -z_0/||z_0||$, $P_{\mathcal{N}}0 = \{z_0\}$ and $J = (p_0, z_0)$. Also $z_0 \in \mathcal{N}(p_0)$. Thus finding the projection of zero $z_0 = P_{\mathcal{N}}0$ is equivalent to the problem (1). The general projection problem can be solved the same way as $P_{\mathcal{N}}x = x + P_{\mathcal{N}+(-x)}0$.

There are many ways to solve the problem of projecting a point onto a convex closed set \mathcal{N} , that depend on how the set \mathcal{N} is defined. If the set \mathcal{N} is a polyhedron, then it can be solved with the help of quadratic programming: min $||x||^2$ under conditions $(p_i, x) \leq s(p_i, \mathcal{N})$, where $\{p_i\}$ is the set

BALASHOV et al.

of unit normals to \mathcal{N} . Method of alternating projections under the transversality condition can be found in [1, Section 8.5]. In [2], the author considers properties of projector operators. They also consider convergence of an iterative projection/reflection algorithm for finding points that achieve a local minimum distance between two closed convex sets or one closed convex set and a closed prox-regular set. Usefulness of conditional gradient-like methods for determining projections onto convex sets was considered in [3]. In [4], the authors proposed an iterative algorithm for metric projection of a point onto a level set of a quadric function. Some algorithms for finding the Bregman projection of a point onto a closed convex set can be found in [5].

The best rate of convergence for the algorithms considered in the papers above is linear. Besides that, in many cases, the considered algorithms do not allow one to obtain an efficient computational procedure.

Further we shall assume that we know supporting function $s(p, \mathcal{N})$ and supporting subset $\mathcal{N}(p)$. "We know" means that we can efficiently compute $s(p, \mathcal{N})$ and $\mathcal{N}(p)$ for any vector $p \in \mathbb{R}^n \setminus \{0\}$.

Suppose that $\mathcal{M} \subset \mathbb{R}^n$ is a convex compact set and $\mathcal{R}(\cdot) : [0,T] \to 2^{\mathbb{R}^n}$, $\mathcal{R}(0) = \{0\}$, is a setvalued mapping with convex compact values that is continuous in Hausdorff metric. Consider a few problems that can be solved in the framework of statement (1).

Problem (P1). For given $t \ge 0$, find the distance between sets $\mathcal{R}(t)$ and \mathcal{M} , i.e. the value of $\rho(\mathcal{R}(t), \mathcal{M}) = \inf_{x \in \mathcal{R}(t), y \in \mathcal{M}} ||x - y||$. Find minimal $t \ge 0$, so that $\rho(\mathcal{R}(t), \mathcal{M}) = 0$.

Problem (P2). For given $t \ge 0$, check whether the inclusion $\mathcal{R}(t) \subset \mathcal{M}$ holds. Find maximal $t \ge 0$, so that $\mathcal{R}(t) \subset \mathcal{M}$.

Problem (P3). For given $t \ge 0$, check whether the inclusion $\mathcal{R}(t) \supset \mathcal{M}$ holds. Find minimal $t \ge 0$, so that $\mathcal{R}(t) \supset \mathcal{M}$.

Problems (P1)–(P3) can be stated for an arbitrary set-valued continuous mapping with convex compact images $\mathcal{R}(t)$ and a convex compact set \mathcal{M} . Consider a particular case of a set-valued integral of the form

$$\mathcal{R}(t) = \int_{0}^{t} \mathcal{F}(s) \, ds, \tag{2}$$

where \mathcal{F} is a set-valued mapping with convex compact values. By default we shall assume that $0 \in \mathcal{F}(s)$ for all $s \ge 0$. The last integral is treated as the Aumann integral [6]

$$\int_{0}^{t} \mathcal{F}(s) \, ds = \left\{ \int_{0}^{t} u(s) \, ds : u(s) \in \mathcal{F}(s) \text{---a measurable selector} \right\}.$$

By the Lyapunov theorem on vector measures [7] the value of the integral is convex and compact. From formula (2) and the inclusion $0 \in \mathcal{F}(s)$ for all $s \in [0, t]$ we conclude that $\{\mathcal{R}(t)\}_{t \ge 0}$ is increasing: $\mathcal{R}(t_1) \subset \mathcal{R}(t_2)$ for all $0 \le t_1 \le t_2$. It is also possible to consider a set $\mathcal{M}(t)$ depending on t.

The support function and supporting subset for integral (2) can be calculated easily: for a unit vector p and any $t \ge 0$ we get

$$s(p,\mathcal{R}(t)) = s\left(p, \int_{0}^{t} \mathcal{F}(s) \, ds\right) = \int_{0}^{t} s\left(p, \mathcal{F}(s)\right) \, ds, \qquad \mathcal{R}(t)(p) = \int_{0}^{t} \mathcal{F}(s)(p) \, ds. \tag{3}$$

Another class of sets for which we know the supporting function and the supporting element are finite sums of linear images of some fixed sets \mathcal{M} with known $s(p, \mathcal{M})$ and $\mathcal{M}(p)$, e.g. ellipsoids. Suppose that $\mathcal{R}(t) = \sum_{k=1}^{m} A_k(t)B_1(0)$, where $A_k(t)$ are continuous nondegenerate matrices for all

 $t \ge 0$. Then

$$s(p,\mathcal{R}(t)) = \sum_{k=1}^{m} s(p,A_k(t)B_1(0)) = \sum_{k=1}^{m} \|A_k^T(t)p\|, \qquad \mathcal{R}(t)(p) = \sum_{k=1}^{m} \frac{A_k(t)A_k^T(t)p}{\|A_k^T(t)p\|}.$$
 (4)

Note that a finite sum of ellipsoids is, in general, not an ellipsoid.

Our most important example is the reachable set of an autonomous linear controlled system, which is described by a differential inclusion

$$x'(t) \in Ax(t) + \mathcal{U}, \ x(0) = 0, \qquad x \in \mathbb{R}^n, \quad A \in \mathbb{R}^{n \times n},$$
(5)

where $\mathcal{U} \subset \mathbb{R}^n$ is a compact, $0 \in \mathcal{U}$. The reachable set (all points to which the system can arrive at the given moment of time) can be represented in the form

$$\mathcal{R}(t) = \int_{0}^{t} e^{As} \mathcal{U} \, ds. \tag{6}$$

The most important strengthening of the convexity condition is the concept of strong convexity with radius R. The set in \mathbb{R}^n is strongly convex with radius R if it can be represented as an intersection of closed balls of radius R [8, 9]. This property can also be defined via the modulus of convexity [10]. In [8], the authors proved that the set-valued integral (2) is strongly convex if the multifunction $\mathcal{F}(s)$ has strongly convex values. In [11], the local strong convexity in certain sense was proved for integral (2) with $\mathcal{F}(s) = A(s)U$, where A(s) is a certain class of smooth matrices and U is a polyhedron. In [12], the second order approximation in time of a Runge-Kutta type scheme for discretization of strongly convex differential inclusions was considered.

Various problems with set-valued integrals can be solved with the help of approximation of values of the integrals. In [13], the authors describe different methods to construct an approximation of the reachable set of a controlled system, see Table 1 therein. One of the most general and effective methods is based on the supporting function (it is also called hyperplane method), see, for example, [14]. We can consider an outer polyhedral approximation for \mathcal{M} of the form

$$\{x \in \mathbb{R}^n : (p, x) \leqslant s(p, \mathcal{M}), \quad \forall p \in \mathbb{G}\},\tag{7}$$

where $\mathbb{G} \subset \mathbb{R}^n$ is a finite grid of unit vectors and solve the problem for the approximation. The disadvantage of this approach is that a reasonable approximation can be obtained only in a space of low dimensions $2 \leq n < 5$, see [15].

There are also different approaches using special approximations, e.g. with zonotopes [16] or ellipsoidal technique [17]. The latter technique sometimes permits to describe the reachable set locally.

In the present paper we think $\mathcal{R}(t)$, \mathcal{M} , \mathcal{N} to be either the value of a set-valued integral or a finite sum of ellipsoids. We shall show how to reduce different problems, e.g. (P1)–(P3), with such sets to the problem (1). The function f(p) in (1) turns out to be the supporting function of some convex compact set \mathcal{N} , which depends on $\mathcal{R}(t)$ and \mathcal{M} . Lezanski-Polyak-Lojasiewicz (LPL) condition [18, formula (4.6)] is proven in problem (1), from which a linear convergence rate for gradient projection algorithm is obtained. The supporting function f(p) and its gradient can be computed, e.g. using formula (3) for a set-valued integral or by (4) for sum of ellipsoids. With the supporting function and its gradient we obtain an efficient calculation scheme. We also consider a local condition of strong convexity: for some R > 0 for the solution p_0 of (1) the inclusion $\mathcal{N} \subset B_R(\mathcal{N}(p_0) - Rp_0)$ holds. Under this condition the problem can be solved with the help of the gradient projection method with a fixed step-size or with Armijo's step-size. We prove a linear rate of convergence for all algorithms and consider various examples.

There is another way to solve (1) using the conditional gradient (CG) method: take the function $g(x) = \frac{1}{2} ||x||^2$, a starting point $x_1 \in \mathcal{N}$ and iterations $\overline{x}_k = \arg \max_{x \in \mathcal{N}} (-g'(x_k), x), x_{k+1} \in$ Arg $\min_{x \in [x_k, \overline{x}_k]} g(x)$. Note that, to ensure the linear convergence of this algorithm, strong convexity of \mathcal{N} is usually required [18, Theorem 6.1, 5].

1.1. Notation and Auxiliary Results

Recall that for sets \mathcal{M} and \mathcal{N} from \mathbb{R}^n we have $\mathcal{M} + \mathcal{N} = \{x + y : x \in \mathcal{M}, y \in \mathcal{N}\}$ and $\mathcal{M} \stackrel{*}{=} \mathcal{N} = \{x : x + \mathcal{N} \subset \mathcal{M}\} = \bigcap_{x \in \mathcal{N}} (\mathcal{M} - x)$. These operations are called the Minkowski sum and difference of sets \mathcal{M} and \mathcal{N} .

Denote by $\varrho(x, \mathcal{M}) = \inf_{y \in \mathcal{M}} ||x - y||$ the distance from a point x to a set \mathcal{M} .

The Hausdorff distance on the space of convex compacts in \mathbb{R}^n can be defined like this: for any convex compact sets $\mathcal{M}, \mathcal{N} \subset \mathbb{R}^n$

$$h(\mathcal{M}, \mathcal{N}) = \max_{\|p\|=1} |s(p, \mathcal{M}) - s(p, \mathcal{N})|.$$

Define $[a]_{-}$: $[a]_{-} = |a|$ for $a \leq 0$ and $[a]_{-} = 0$ for a > 0. Then $[\min_{\|p\|=1}(s(p, \mathcal{M}) - s(p, \mathcal{N}))]_{-}$ is the half distance from \mathcal{N} to \mathcal{M} and it is equal to $\max_{x \in \mathcal{N}} \varrho(x, \mathcal{M})$.

Suppose that the set $\mathcal{R}(t)$ (6) depends on parameter t. Then we shall denote the supporting set for a vector p by $\mathcal{R}(t)(p)$. From the Aumann's or Riemann's definition of the integral for any matrix $J \in \mathbb{R}^{m \times n}$ we have $J\mathcal{R}(t) = \int_0^t J e^{As} \mathcal{U} \, ds$. In particular, for any vector $p \in \mathbb{R}^n$

$$\mathcal{R}(t)(p) = \int_{0}^{t} (e^{As}\mathcal{U})(p) \, ds.$$

A set $\mathcal{M} \subset \mathbb{R}^n$ is strongly convex with radius R > 0 if we can represent \mathcal{M} as intersection of some collection of closed Euclidean balls with radius R. For any strongly convex set \mathcal{M} with radius R > 0 there exists another strongly convex set \mathcal{N} with radius R such that $\mathcal{M} + \mathcal{N} = \mathcal{B}_R(0)$ [8, 19]. Strong convexity of a compact convex set \mathcal{M} with radius R is equivalent to the Lipschitz condition for the supporting element $\mathcal{M}(p)$ on the unit sphere: for all ||p|| = ||q|| = 1 we have $||\mathcal{M}(p) - \mathcal{M}(q)|| \leq R||p - q||$ [8].

We shall say that a convex set $\mathcal{M} \subset \mathbb{R}^n$ is uniformly smooth with constant r > 0 if we have $\mathcal{M} = \mathcal{M}_0 + \mathcal{B}_r(0)$, where $\mathcal{M}_0 \subset \mathbb{R}^n$ is a convex compact set. For more details see [20, Definition 2.1].

Let $\mathcal{S}_0 \subset \mathbb{R}^n$ be a smooth manifold without boundary, $\overline{x} \in \mathcal{S}_0$, $\varepsilon > 0$. For a differentiable function $f: \mathcal{S}_0 + \operatorname{int} \mathcal{B}_{\varepsilon}(0) \to \mathbb{R}$ define $\mathcal{S} = \mathcal{S}(f, \overline{x}) = \{x \in \mathcal{S}_0 : f(x) \leq f(\overline{x})\}$. Assume \mathcal{S} to be a smooth manifold with the boundary $\partial \mathcal{S} \subset \{x \in \mathcal{S}_0 : f(x) = f(\overline{x})\}$. We shall say that the Lezanski– Polyak–Lojasiewicz (LPL) condition holds on \mathcal{S} [18; 21, Section 3.2] with a constant $\mu > 0$ if $\Omega = \operatorname{Arg\,min}_{x \in \mathcal{S}} f(x) \neq \emptyset$ and for all $x \in \mathcal{S}$ the following inequality holds

$$\|P_{\mathcal{T}_x}f'(x)\|^2 \ge \mu(f(x) - f(\Omega)). \tag{(\star)}$$

Here \mathcal{T}_x is the tangent subspace to the manifold \mathcal{S} at the point $x \in \mathcal{S}$, $P_{\mathcal{T}_x}$ is the orthogonal projector onto \mathcal{T}_x , f'(x) is the Frechet gradient of the function f at the point $x \in \mathcal{S}$.

Lemma 1. For any nonzero vectors $p, q \in \mathbb{R}^n$ we have $\left\| \frac{p}{\|p\|} - \frac{q}{\|q\|} \right\| \leq \frac{\|p-q\|}{\sqrt{\|p\| \|q\|}}$,

Proposition 1 [8]. Suppose that a set-valued mapping $\mathcal{F} : [0,t] \to 2^{\mathbb{R}^n}$ is continuous in the Hausdorff metric and has strongly convex images $\mathcal{F}(s)$ with radius R(s) for all $s \in [0,t]$, that is integrable at [0,t]. Then the integral $\mathcal{P} = \int_0^t F(s) ds$ is strongly convex with radius $R = \int_0^t R(s) ds$.

It should be mentioned that the set-valued integral can be strongly convex even when $\mathcal{F}(s)$ is not. itself. For example, this situation typically takes place for the reachable set $\mathcal{R}(t)$ of system (5) in dimension n = 2 [22]. Nevertheless, the reachable set in dimensions $n \ge 3$ is often not strongly convex. Let us look at an elementary example of a system mentioned in (5) (a similar system is considered in Example 1 below). Let the control set be a segment: $\mathcal{U} = \operatorname{co} \{\pm v\}$. Define an analytic function $g_p(s) = (p, e^{As}v)$. The supporting set $\mathcal{R}(t)(p)$ is a singleton, provided that $g_p(s) \neq 0$. This is guaranteed by full rank conditions

$$\operatorname{span}\{A^{i}v\}_{i=0}^{n-1} = \mathbb{R}^{n} \quad \Leftrightarrow \quad \operatorname{span}\mathcal{R}(t) = \mathbb{R}^{n}$$

Since g_p is analytic, the equation $g_p = 0$ has a finite number of roots in [0, t]. The supporting element can be written down as

$$\mathcal{R}(t)(p) = \int_{0}^{t} e^{As} v \times \operatorname{sign} g_{p}(s) \, ds = \sum_{i=0}^{k} \epsilon_{i} \int_{s_{i}(p)}^{s_{i+1}(p)} e^{As} v \, ds, \tag{8}$$

where $s_i(p)$, $i = \overline{1, k}$ are the roots of $g_p(s)$, $s_0 = 0$, $s_{k+1} = t$, $\epsilon_i = \pm 1$ is equal to sign of $g_p(s)$ when $s \in [s_i, s_{i+1}]$. Therefore, the behaviour of supporting element is defined by dependence of roots of analytic function $g_p(s)$ on parameter p. If all roots are simple and lie on interval (0, t), then it follows from implicit function theorem that the support element depends smoothly on p in the neighbourhood. Therefore, the supporting element is locally Lipschitz. On the other hand, g_p can have roots with multiplicity greater than one belonging to [0, t]. In this case the supporting element is typically not locally Lipschitz, which means that the strong convexity fails. This is illustrated in the example below. However, it is easy to show the set of vectors p, such that g_p has non-simple zeros on [0, t], has measure zero on the unit sphere. Some generalizations of this approach to set-valued integrals can be seen in [11].

Note that if all eigenvalues of A are real, then the number of switchings in optimal control $u(t) = \mathcal{U}(e^{A^T(T-t)}p) = v \times \operatorname{sgn} g_p(T-t)$ is no greater than n-1, it is a special case of Feldbaum theorem, see [23, Theorem 2.11]. In the examples below, we consider a dynamical system defined by $\dot{x} = Ax + Bu$, $u \in \mathcal{U}$, $t \in [0, T]$. The optimal control that guides the system to the support element $\mathcal{R}(t)(p)$ is [24]:

$$u(t) = \mathcal{U}(B^{\top} e^{A^{\top}(T-t)}), \quad t \in [0,T].$$
(9)

Consider the system

$$\dot{x} = Ax + Bu, \quad x(0) = 0, \quad u \in \mathbb{R}: \quad |u| \leq 1, \quad A = \begin{bmatrix} -1 & 1 & 0 \\ 0 & -1 & 1 \\ 0 & 0 & -1 \end{bmatrix}, \quad B = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}.$$
 (10)

Following what was said above, let $g_p(s) = (p, e^{As}B) = \frac{1}{2}e^{-s}(p_1s^2 + 2p_2s + 2p_3).$

Let $p_0 = \frac{1}{3}(2, -2, 1)$, note that $g_{p_0}(s) = \frac{1}{3}e^{-s}(s-1)^2$ has a multiple root s = 1. We are interested in behaviour of supporting element near p_0 . Remember that $f(s) \simeq g(s), s \to 0$, if f(s) = O(g(s))and $g(s) = O(f(s)), s \to 0$. Define for $\varepsilon \in (0, 1)$ a unit vector $q = q(\varepsilon) = \frac{(2, -2, 1-\varepsilon)}{\sqrt{9-2\varepsilon+\varepsilon^2}}$. It is easy to see that $\|p - q(\varepsilon)\| \simeq \varepsilon, \varepsilon \to 0$, and to find the roots $g_{q(\varepsilon)} =: s_{1,2}(\varepsilon) = 1 \pm \sqrt{\varepsilon}$. Then for $t > 1 + \sqrt{\varepsilon}$ we can write down the supporting element in the following way:

$$\mathcal{R}(t)(p) - \mathcal{R}(t)(q) = \int_{1-\sqrt{\varepsilon}}^{1+\sqrt{\varepsilon}} e^{-s} (s^2, \ 2s, \ 2)^\top \, ds,$$
$$\|\mathcal{R}(t)(p) - \mathcal{R}(t)(q)\| \ge \int_{1-\sqrt{\varepsilon}}^{1+\sqrt{\varepsilon}} 2e^{-s} \, ds \asymp \sqrt{\varepsilon}, \ \varepsilon \to 0.$$

Therefore, the supporting element fails to be Lipschitz in a neighbourhood of p_0 , so the reachable set $\mathcal{R}(t)$ is not strongly convex.



Fig. 1. Attainable set of (10) and normal vectors, where the supporting element is not locally Lipschitz, t = 2.

The reachable set for t = 2 can be seen at Fig. 1. Normal vectors, for which the supporting element is not locally Lipschitz, can be seen in the upper part of the figure. They lie on the boundary of the normal cone at the tip of the set. Moreover, it is evident that the reachable set is structured like a CW complex. This structure appears as a result of (8), since the supporting element can be determined by positions and multiplicities of the roots of $g_p(s)$ on [0, t] and the sign of g_p around the left end of the segment. If the system has a matrix with real eigenvalues, then the overall multiplicity of roots of g_p is not greater that n - 1. It can be shown, that in this case an arbitrary configuration of roots substituted into (8) produces a point from $\partial Rs(t)$. Evaluating (8) on sets of roots with different overall multiplicities allows us to extract curvilinear edges and faces from the reachable set. Some generalization of the above arguments can be seen in [11].

Lemma 2. Suppose that $A_1 = J^{-1}AJ$ is the Jordan form of the matrix A from system (5), $\mathcal{U}_1 = J^{-1}\mathcal{U}$, where $J \in \mathbb{R}^{n \times n}$ is the transfer matrix. If the set $\mathcal{R}_1(t) = \int_0^t e^{A_1s}\mathcal{U}_1 ds$ is strongly convex with radius r, then $\mathcal{R}(t) = \int_0^t e^{As}\mathcal{U} ds$ is also strongly convex with radius $R = r\alpha^2/\beta$, where $\alpha = \|J\| = \max_{\|h\|=1} \|Jh\|$, $\beta = \min_{\|h\|=1} \|Jh\|$.

Note that by [25, Theorem 3] any ellipsoid

$$\mathcal{N} = \left\{ x \in \mathbb{R}^n : \sum_{k=1}^n \frac{x_k^2}{\lambda_k^2} \leqslant 1 \right\}, \quad \lambda_1 \ge \lambda_2 \ge \ldots \ge \lambda_n > 0,$$

is strongly convex with radius $R = \frac{\lambda_1^2}{\lambda_n}$.

Lemma 3. Suppose that in system (5) \mathcal{U} is uniformly smooth with constant r > 0. Then $\mathcal{R}(t)$ (6) is uniformly smooth with constant $r_0 = r \int_0^t \frac{\lambda_n^2(s)}{\lambda_1(s)} ds$, where $\lambda_1(s) \ge \ldots \ge \lambda_n(s) > 0$ are the semiaxes of the ellipsoid $e^{As} \mathcal{B}_1(0)$.

Note that by the proof of Lemma 3 any ellipsoid

$$\mathcal{N} = \left\{ x \in \mathbb{R}^n : \sum_{k=1}^n \frac{x_k^2}{\lambda_k^2} \leqslant 1 \right\}, \quad \lambda_1 \ge \lambda_2 \ge \ldots \ge \lambda_n > 0,$$

is uniformly smooth with constant $r = \frac{\lambda_n^2}{\lambda_1}$.

In particular, Lemmas 2 and 3 show that it is enough to consider system (5) with the Jordan form of the matrix A.

The next proposition estimates the rate of decrease for a Lipschitz differentiable function per step of the gradient projection method.

Proposition 2 [26, Lemma 2]. Consider the problem $\min_{\mathcal{M}} f(x)$ in \mathbb{R}^n . Suppose that \mathcal{M} is a closed set, f' is a Lipschitz function with constant L_1 . Fix $0 < \lambda \leq \frac{1}{L_1}$. Assume that $x_0 \in \mathcal{M}$ and $y_0 \in P_{\mathcal{M}}(x_0 - \lambda f'(x_0))$. Then

$$f(x_0) - f(y_0) \ge \frac{1}{2} \left(\frac{1}{\lambda} - L_1\right) \|x_0 - y_0\|^2.$$

For the validity of the previous formula the Lipschitz condition for f' with constant L_1 is essential on the segment $[x_0, y_0]$, see the proof of [27, Proposition 2.2].

1.2. Additional Assumptions on $\mathcal{R}(s)$

When solving problems (P1)-P(3) we will require some additional assumptions on sets we work with. Here we will enumerate all of them, we will only need some of them for each problem.

- (1) $\mathcal{R}(s)$ is strongly convex with radius $R_T > 0$ for all $s \in [0, T]$.
- (2) \mathcal{M} is uniformly smooth with constant r > 0: $\mathcal{M} = \mathcal{M}_0 + \mathcal{B}_r(0)$, also
 - (a) \mathcal{M}_0 us strongly convex with constant $R_0 > 0$.
 - (b) $r > R_T$.
- (3) \mathcal{M} is strongly convex with constant $R_0 > 0$.
- (4) \mathcal{U} is uniformly smooth with constant $r_{\mathcal{U}} > 0$: $\mathcal{U} = \mathcal{U}_0 + \mathcal{B}_{r_{\mathcal{U}}}(0)$.
- (5) $r(t) > R_0$, where $r(t) = r_{\mathcal{U}} \int_0^t \frac{\lambda_n^2(s)}{\lambda_1(s)}$ and $\lambda_1(s) \ge \ldots \ge \lambda_n(s)$ are the semiaxes of the ellipsoid $e^{As} \mathcal{B}_1(0)$.

The first assumption is fulfilled if, for example, the set $e^{As}\mathcal{U}$ is strongly convex with radius R(s) > 0. Then from proposition 1 and linearity of the integral it follows that

$$\mathcal{R}(T) = \int_{0}^{T} e^{As} \mathcal{U} \, ds = \int_{0}^{t} e^{As} \mathcal{U} \, ds + \int_{t}^{T} e^{As} \mathcal{U} \, ds = \mathcal{R}(t) + \int_{t}^{T} e^{As} \mathcal{U} \, ds,$$

then we obtain that the set

$$\mathcal{R}(t) = \bigcap \left\{ \mathcal{R}(T) - x : x \in \int_{t}^{T} e^{As} \mathcal{U} \, ds \right\}$$

is strongly convex with radius $R_T = \int_0^T R(s) ds$ for all $t \in [0, T]$.

1.3. Structure of the Paper

In Sections 2–4 we formulate sufficient conditions and prove results about linear convergence of the gradient projection method for a particular optimization problem with supporting functions to which problems (P1)–(P3) are reduced. This solves problems for a fixed $t \in [0, T]$.

In Section 5 we discuss how we can find the starting point p_1 for the iteration process. Estimates of the probability of finding p_1 using random search are given.

In Section 6 we discuss the results of numerical experiments. Here we also consider an algorithm for finding the optimal t in problems (P1)–(P3).

BALASHOV et al.

2. PROBLEM (P1)

Assumptions: 1, 2(a).

For all $t \in [0, T]$ consider the set $\mathcal{N}(t) = \mathcal{R}(t) + (-\mathcal{M}_0)$. The set $\mathcal{N}(t)$ is strongly convex with radius $R = R_T + R_0$ as a sum of strongly convex sets [19]. The equality $\mathcal{R}(t) \cap \mathcal{M} = \emptyset$ can be reformulated as follows: the distance from zero to $\mathcal{N}(t)$ is more than r > 0. If the last assertion is true, then $0 \notin \mathcal{R}(t) + (-\mathcal{M})$ and otherwise $0 \in \mathcal{R}(t) + (-\mathcal{M})$. Using the supporting function we can check the inclusion as follows: for the function $f(p) = s(p, \mathcal{N}(t)) = s(p, \mathcal{R}(t)) + s(p, -\mathcal{M}_0)$ find

$$\min_{\|p\|=1} f(p) = J.$$
(11)

If J < -r, then the distance from zero to the set $\mathcal{N}(t)$ is greater than r. If $J \ge -r$, then the distance from zero to the set $\mathcal{N}(t)$ is no greater than r and hence $0 \in \mathcal{R}(t) + (-\mathcal{M})$. Note that

$$f'(p) = \mathcal{R}(t)(p) + (-\mathcal{M}_0)(p) = \int_0^t (e^{As}\mathcal{U})(p) \, ds + (-\mathcal{M}_0)(p).$$
(12)

Theorem 1. Fix $\varepsilon \in (0,1)$. Suppose that in (11) J < 0. Then under above mentioned assumptions the function f in (11) satisfies the LPL condition on the manifold $S = \{p \in S_1 : f(p) \leq 0\}$ with constant $\mu = |J|$. Also the function f has Lipschitz continuous gradient on the set $\{p \in \mathbb{R}^n : 1 - \varepsilon \leq ||p|| \leq 1 + \varepsilon\}$ with Lipschitz constant $L_1 = \frac{R}{1-\varepsilon} = \frac{R_T + R_0}{1-\varepsilon}$.

Consider the following iteration process

$$p_1 \in \mathcal{S} \text{ (i.e. } f(p_1) \leq 0), \quad p_{k+1} = P_{\mathcal{S}_1}(p_k - \lambda f'(p_k)), \qquad \lambda \in \left(0, \frac{1}{L_1}\right].$$
 (13)

If $p_k \in \mathcal{S}$, then $p_{k+1} \in \mathcal{S}$. Indeed, by Proposition 2

$$f(p_k) - f(p_{k+1}) \ge \frac{1}{2} \left(\frac{1}{\lambda} - L_1\right) \|p_k - p_{k+1}\|^2 \ge 0, \quad f(p_{k+1}) \le f(p_k) \le 0$$

Consider the point $p_k - \lambda f'(p_k)$. We have

$$||p_k - \lambda f'(p_k)|| \ge (p_k, p_k - \lambda f'(p_k)) = 1 - \lambda (p_k, f'(p_k)) = 1 - \lambda f(p_k) \ge 1.$$

Theorem 2. Suppose that the function f is Lipschitz continuous with constant $L = ||\mathcal{N}(t)||$, the function f' is Lipschitz continuous on S_1 with constant $R = R_T + R_0$. Suppose that J < 0. Put $L_1 = 2R$.

Fix $\lambda \in (0, \min\{\frac{1}{L_1}, \frac{1}{2L}\})$. Then algorithm (13) converges to a point of minimum $p_0 \in S_1$ at a linear rate:

$$f(p_{k+1}) - f(p_0) \leqslant q(f(p_k) - f(p_0)),$$

$$\|p_{k+1} - p_k\| \leqslant q^{k/2} \sqrt{2\lambda(f(p_1) - f(p_0))},$$

$$q = 1 - \frac{\lambda|J|}{2L\lambda + 2} \in (0, 1).$$

The next example shows that the sharpness condition of the type $\exists \alpha > 0$ that $f(p) - f(p_0) \ge \alpha \|p - p_0\|$ for all $p \in S$ does not hold.

Consider L > r > 0, $||p_0|| = 1$ and the set $\mathcal{N} = \mathcal{B}_r(-Lp_0)$. Then for all $p \in \mathcal{S}_1$ we have

$$s(p, \mathcal{N}) - s(p_0, \mathcal{N}) = L(1 - (p, p_0)) = \frac{L}{2} ||p - p_0||^2$$

Remark 1. The above results can be proven under more local assumptions. Instead of the strong convexity assumption 1 of $\mathcal{R}(T)$ with radius R_T we can require the fulfillment for all $p \in S$ the supporting principle for the set $\mathcal{R}(t)$: there exists $R_T > 0$ with

$$\mathcal{R}(t) \subset B_{R_T}(\mathcal{R}(t)(p) - R_T p), \quad \forall p \in \mathcal{S}.$$
 (14)

Assumption 2(a) concerning \mathcal{M} must be met.

In this situation the set $Z(t) = \mathcal{R}(t) + (-\mathcal{M}_0)$ satisfies the supporting principle for all $p \in S$ with radius $R = R_T + R_0$:

$$Z(t) \subset B_R(\mathcal{N}(t)(p) - Rp), \quad \forall p \in \mathcal{S}.$$

For any $p, q \in \mathcal{S}$ we get $\|\mathcal{N}(t)(p) - Rp - \mathcal{N}(t)(q)\|^2 \leq R^2$, $\|\mathcal{N}(t)(q) - Rq - \mathcal{N}(t)(p)\|^2 \leq R^2$ and $\|\mathcal{N}(t)(p) - \mathcal{N}(t)(q)\|^2 \leq 2R(p, \mathcal{N}(t)(p) - \mathcal{N}(t)(q))$,

$$\|\mathcal{N}(t)(q) - \mathcal{N}(t)(p)\|^2 \leq 2R(q, \mathcal{N}(t)(q) - \mathcal{N}(t)(p)) = 2R(-q, \mathcal{N}(t)(p) - \mathcal{N}(t)(q)),$$

hence $\|\mathcal{N}(t)(p) - \mathcal{N}(t)(q)\| \leq R \|p - q\|$. Keeping in mind that for any $p, q \in S$ the small arc of the circle of radius 1 with center 0 and endpoints p, q belongs to S, we can repeat proofs of Theorems 1 and 2 for the considered case. In the generalization of Theorem 1 we should take $p, q \in \mathbb{R}^n$ with $\frac{p}{\|p\|}$, $\frac{q}{\|q\|} \in S$, i.e. Lipschitz condition will be proved on the set $\left\{p \in \mathbb{R}^n : 1 - \varepsilon \leq \|p\| \leq 1 + \varepsilon, \frac{p}{\|p\|} \in S\right\}$.

3. PROBLEM (P2)

Assumptions: 1, 2(b), 3.

Fix $\varepsilon \in (0, r - R_T)$. Consider ε -neighbourhood $\mathcal{R}_{\varepsilon}(t) = \mathcal{R}(t) + \mathcal{B}_{\varepsilon}(0)$ of the set $\mathcal{R}(t)$. Inclusion $\mathcal{R}(t) \subset \mathcal{M}$ means that

$$\max_{x \in \mathcal{R}_{\varepsilon}(t)} \varrho(x, \mathcal{M}) \leqslant \varepsilon$$

and otherwise, if $\max_{x \in \mathcal{R}_{\varepsilon}(t)} \varrho(x, \mathcal{M}) > \varepsilon$, then $\mathcal{R}(t) \not\subset \mathcal{M}$. Using supporting functions we can formulate an equivalent problem: for the function $f(p) = s(p, \mathcal{M}) - s(p, \mathcal{R}_{\varepsilon}(t))$ find minimum

$$\min_{\|p\|=1} f(p) = J.$$
(15)

If $J \ge -\varepsilon$ then $\mathcal{R}(t) \subset \mathcal{M}$ and if $J < -\varepsilon$ then $\mathcal{R}(t) \not\subset \mathcal{M}$.

Let $S = \{p \in S_1 : f(p) \leq 0\}$. Suppose that $p_0 \in S_1$ is a solution of (15).

Assume that $\mathcal{S} \neq \emptyset$. Consider an iteration process

$$p_1 \in \mathcal{S}, \qquad p_{k+1} = P_{\mathcal{S}_1}(p_k - \lambda f'(p_k)). \tag{16}$$

Theorem 3. Suppose that under assumptions of Section 3 we have J < 0 in problem (15). Let $r_0 = r - R_T - \varepsilon > 0$, $L = ||\mathcal{M} \stackrel{*}{\to} \mathcal{R}_{\varepsilon}(t)|| > 0$. Then for any $p_1 \in S$ and $0 < \lambda \leq \min\{r_0^2/R_0^3, 1/(2L), 1/(2R_0)\}$ iterations (16) converge at a linear rate to the solution p_0 :

$$||p_{k+1} - p_0|| \leq q ||p_k - p_0||, \qquad q = \sqrt{1 - \frac{2r_0^2}{R_0}\lambda + R_0^2\lambda^2} \in (0, 1)$$

Remark 2. As in Section 2, we can prove the above results under more local assumptions. Instead of the Assumption 1 on strong convexity of $\mathcal{R}(s)$ for all $s \in [0,T]$ with radius R_T we can require the fulfillment for all $p \in S$ of the supporting principle for the set $\mathcal{R}(t)$: there exists $R_T > 0$ such that for a number $\varepsilon \in (0, r - R_T)$ we have

$$\mathcal{M}(p) - \mathcal{R}(t)(p) + \mathcal{R}(t) \subset B_{R_T}(\mathcal{M}(p) - R_T p) \subset B_{r-\varepsilon}(\mathcal{M}(p) - (r-\varepsilon)p) \subset \mathcal{M}, \quad \forall p \in \mathcal{S}.$$
(17)

Assumptions 2(b), 3 concerning \mathcal{M} must be met.

In the considered situation we have

$$\mathcal{M}(p) - \mathcal{R}(t)(p) - \varepsilon p + \mathcal{R}_{\varepsilon}(t) \subset \mathcal{M}, \quad \forall p \in \mathcal{S}$$
(18)

and hence $f'(p) = \mathcal{M}(p) - \mathcal{R}(t)(p) - \varepsilon \times p = \mathcal{M}(p) - \mathcal{R}_{\varepsilon}(t)(p) = (\mathcal{M}^{*} - \mathcal{R}_{\varepsilon}(t))(p)$ for all $p \in \mathcal{S}$ because $f'(p) \in \mathcal{M}^{*} - \mathcal{R}_{\varepsilon}(t)$ and $(p, f'(p)) = s(p, \mathcal{M}^{*} - \mathcal{R}_{\varepsilon}(t))$ for all $p \in \mathcal{S}$. Indeed, fix $p \in \mathcal{S}$. From the inclusion $f'(p) + \mathcal{R}_{\varepsilon}(t) \subset \mathcal{M}$ we get $f'(p) \in \mathcal{M}^{*} - \mathcal{R}_{\varepsilon}(t)$. On the other hand $(p, f'(p)) + s(p, \mathcal{R}_{\varepsilon}(t)) = s(p, \mathcal{M})$ and thus $(p, f'(p)) = s(p, \mathcal{M}) - s(p, \mathcal{R}_{\varepsilon}(t)) \ge co(s(p, \mathcal{M}) - s(p, \mathcal{R}_{\varepsilon}(t)) = s(p, \mathcal{M}^{*} - \mathcal{R}_{\varepsilon}(t))$.

The next steps repeat the proof of Theorem 3.

4. PROBLEM (P3)

Assumptions: 1, 3, 4, 5.

Note that by Lemma 3 the set $\mathcal{R}(t)$ is uniformly smooth with constant r(t) and hence $R_T \ge r(t)$. Fix $\varepsilon \in (0, r(t) - R_0)$. Consider ε -neighbourhood $\mathcal{M}_{\varepsilon} = \mathcal{M} + \mathcal{B}_{\varepsilon}(0)$ of the set \mathcal{M} . Inclusion $\mathcal{R}(t) \supset \mathcal{M}$ means that

$$\max_{x \in \mathcal{M}_{\varepsilon}} \varrho(x, \mathcal{R}(t)) \leqslant \varepsilon$$

and otherwise, if $\max_{x \in \mathcal{M}_{\varepsilon}} \varrho(x, \mathcal{R}(t)) > \varepsilon$, then $\mathcal{R}(t) \not\supseteq \mathcal{M}$. On the base of supporting functions we can formulate the next equivalent problem: for the function $f(p) = s(p, \mathcal{R}(t)) - s(p, \mathcal{M}_{\varepsilon}) = s(p, \mathcal{R}(t)) - s(p, \mathcal{M}) - \varepsilon \|p\|$ find minimum

$$\min_{\|p\|=1} f(p) = J.$$
(19)

If $J \ge -\varepsilon$ then $\mathcal{R}(t) \supset \mathcal{M}$ and if $J < -\varepsilon$ then $\mathcal{R}(t) \not\supset \mathcal{M}$.

As usual, $S = \{p \in S_1 : f(p) \leq 0\}$. Suppose that $p_0 \in S_1$ is a solution of (19). Assume that $S \neq \emptyset$. Consider an iteration process

$$p_1 \in \mathcal{S}, \qquad p_{k+1} = \mathcal{P}_{\mathcal{S}_1}(p_k - \lambda f'(p_k)).$$
 (20)

Theorem 4. Suppose that under assumptions of Section 4 we have J < 0 in problem (19). Let $r = r(t) - R - \varepsilon > 0$, $L = ||\mathcal{R}(t) \stackrel{*}{\longrightarrow} \mathcal{M}_{\varepsilon}||$. Then for any $p_1 \in S$ and $0 < \lambda \leq \min\{r^2/R_T^3, 1/(2L), 1/(2R_T)\}$ iterations (20) converges at a linear rate to the solution p_0 :

$$||p_{k+1} - p_0|| \leq q ||p_k - p_0||, \qquad q = \sqrt{1 - \frac{2r^2}{R_T}\lambda + R_T^2\lambda^2} \in (0, 1).$$

Remark 3. As in Section 3, we can also prove the above results under more local assumptions. Instead of the strong convexity Assumption 3 of \mathcal{M} with radius R_0 we can require the fulfillment for all $p \in \mathcal{S}$ of the supporting condition for the set \mathcal{M} : there exists $R_0 > 0$ such that

$$\mathcal{M} \subset B_{R_0}(\mathcal{M}(p) - R_0 p), \quad \forall p \in \mathcal{S}.$$
 (21)

Assumptions 1, 4 and 5 must be met.

5. CHOOSING THE INITIAL POINT

We choose p_1 using random search: in problems (P1)–(P3) we sample a random vector $p_1 \in S_1$ from a uniform distribution and check the inequality $f(p_1) \leq 0$. If it fails, we choose another random vector $p_1 \in S_1$ and so on. In the present section we estimate the probability $\mathbb{P}(\{f(p_1) \leq 0\})$ to find an appropriate vector p_1 . As an example, let us consider (P1) for fixed t > 0. Recall, that

J < 0 is the solution of problem (11). By assumptions for (P1), the set $\mathcal{N}(t)$ is strongly convex with radius R > 0. Denote $z_0 = P_{\mathcal{N}(t)}0$, $p_0 = -z_0/||z_0||$. For a set $\mathcal{M} \subset \mathbb{R}^n$ define cone \mathcal{M} to be the (convex) conic hull of the set \mathcal{M} , i.e. cone $\mathcal{M} = \{\sum_{i=1}^n \lambda_i x_i : x_i \in \mathcal{M}, \lambda_i \ge 0\}$. For a pair of points $x, y \in \mathbb{R}^n, x \ne y$, define the ray $[x, y) = \{x + t(y - x) : t \ge 0\}$.

Let D > 0 and $H = \{x \in \mathbb{R}^n : (p_0, x - z_0) = 0\}$. Suppose that $\mathcal{K} = \text{cone } (H \cap B_D(z_0)) \supset \text{cone } \mathcal{N}(t)$. For example, D can be the diameter of the set $\mathcal{N}(t)$, i.e. $D = \sup_{x,y \in \mathcal{N}(t)} ||x - y||$.

The set \mathcal{K} is a cone of revolution with axis $[0, z_0)$. The angle between the axis and a generatrix is equal to α , $\tan \alpha = \frac{D}{|J|}$. The polar set $\mathcal{K}^- = \{p \in \mathbb{R}^n : (p, q) \leq 0 \quad \forall q \in \mathcal{K}\}$ is also a cone of revolution with axis $[0, -z_0)$ and the angle between the axis and a generatrix is equal to $\beta = \frac{1}{2}\pi - \alpha$, thus $\cos \beta = \frac{D}{\sqrt{D^2 + J^2}}$.

By the definition of \mathcal{K} we have for any $p_1 \in \mathcal{S}_1 \cap \mathcal{K}^-$ that $f(p_1) \leq 0$. Denote $\mathcal{S}_{\operatorname{cap}} = \mathcal{S}_1 \cap \mathcal{K}^$ and $\mathcal{S}_0 = \mathcal{K}^- \cap H_0$, here $H_0 = \{x \in \mathbb{R}^n : (p_0, x) = \cos\beta\}$. Note that $\mathcal{S}_0 = H_0 \cap B_{r_0}(\cos\beta \times p_0)$ with $r_0 = \sin\beta = \frac{|J|}{\sqrt{D^2 + J^2}}$. (n-1)-Lebesgue's measure $\mu_{n-1}\mathcal{S}_0 \leq \mu_{n-1}\mathcal{S}_{\operatorname{cap}}$ and thus

$$\mathbb{P}(\{f(p_1) \leqslant 0\}) \geqslant \frac{\mu_{n-1}\mathcal{S}_{\text{cap}}}{\mu_{n-1}\mathcal{S}_1} \geqslant \frac{\mu_{n-1}\mathcal{S}_0}{\mu_{n-1}\mathcal{S}_1} = \frac{r_0^{n-1}}{n} \frac{V_{n-1}}{V_n} = \frac{1}{n} \frac{V_{n-1}}{V_n} \left(\frac{|J|}{\sqrt{D^2 + J^2}}\right)^{n-1}$$

 $V_n = \frac{\pi^{n/2}}{\Gamma(\frac{n}{2}+1)}$ is the volume of a unit ball in \mathbb{R}^n .

Suppose now that $B_r(z_0 - rp_0) \subset \mathcal{N}(t)$ for some r > 0. Then consider a cone of revolution $\mathcal{K} = \operatorname{cone} B_r(z_0 - rp_0) \subset \operatorname{cone} \mathcal{N}(t)$ with axis $[0, z_0)$. The angle between the axis and a generatrix of \mathcal{K} is equal to α , $\sin \alpha = \frac{r}{r+|\mathcal{J}|}$. Define a polar cone $\mathcal{K}^- \supset (\operatorname{cone} \mathcal{N}(t))^-$ with the angle β between the axis $[0, -z_0)$ and a generatrix, $\cos \beta = \frac{r}{r+|\mathcal{J}|}$. We have for any $p_1 \in \mathcal{S}_1$ with $f(p_1) \leq 0$ that $p_1 \in \mathcal{S}_{\operatorname{cap}}$, as previously $\mathcal{S}_{\operatorname{cap}} = \mathcal{S}_1 \cap \mathcal{K}^-$. Define $\mathcal{S}_0^1 = \mathcal{K}^- \cap H_1$ with $H_1 = \{x \in \mathbb{R}^n : (p_0, x) = 1\}$. From the elementary planimetry it is easy to see that $\mathcal{S}_0^1 = H_1 \cap B_{r_1}(p_0), r_1 = \tan \beta = \frac{\sqrt{2r|\mathcal{J}| + |\mathcal{J}|^2}}{r}$. Then $\mu_{n-1}\mathcal{S}_0^1 \geq \mu_{n-1}\mathcal{S}_{\operatorname{cap}}$ and

$$\mathbb{P}(\{f(p_1) \leqslant 0\}) \leqslant \frac{\mu_{n-1}\mathcal{S}_{cap}}{\mu_{n-1}\mathcal{S}_1} \leqslant \frac{\mu_{n-1}\mathcal{S}_0^1}{\mu_{n-1}\mathcal{S}_1} = \frac{r_1^{n-1}}{n} \frac{V_{n-1}}{V_n} = \frac{1}{n} \frac{V_{n-1}}{V_n} \left(\frac{\sqrt{2r|J| + |J|^2}}{r}\right)^{n-1}.$$

Finally for a set $\mathcal{N}(t)$ of diameter D that is also uniformly smooth with constant r we have

$$\frac{1}{n} \frac{V_{n-1}}{V_n} \left(\frac{|J|}{\sqrt{D^2 + J^2}}\right)^{n-1} \leqslant \mathbb{P}(\{f(p_1) \leqslant 0\}) \leqslant \frac{1}{n} \frac{V_{n-1}}{V_n} \left(\frac{\sqrt{2r|J| + |J|^2}}{r}\right)^{n-1}.$$
(22)

Similarly with the right estimate in (22) for an R-strongly convex set $\mathcal{N}(t)$ one can prove that

$$\frac{1}{n}\frac{V_{n-1}}{V_n}\left(\frac{\sqrt{2R|J|+|J|^2}}{R+|J|}\right)^{n-1} \leqslant \mathbb{P}(\{f(p_1)\leqslant 0\})$$

This estimate shows that $\mathbb{P}(\{f(p_1) \leq 0\}) \simeq |J|^{n-1}$ when $J \to 0$. In our consideration |J| is of the order $\varepsilon > 0$ and in this case the left inequality in (22) gives a more reasonable estimate because in most examples the value of D is much less than R.

The estimated probability can be very small and strongly influences calculations when either |J| is close to zero or n is large. In our experiments in the examples below for n in range $3 \le n \le 12$ we found p_1 in a few dozens attempts at most (for problems (P1), (P2)). Sometimes we needed about 1000 attempts to find the vector p_1 in problem (P3). One of the reasons is that D > 0 in the above estimate can be chosen to be significantly smaller than the diameter $\mathcal{N}(t)$, since we only need the fulfillment of the inclusion cone $(H \cap B_D(z_0)) \supset \operatorname{cone} \mathcal{N}(t)$.

BALASHOV et al.

Sometimes we can choose p_1 deterministically, see the Algorithm from Section 9.

The step size λ for solving problems (P1)–(P3) can be chosen using the Armijo rule. Its detailed description can be found in [29].

6. MODELING AND EXAMPLES

Some of the considered examples are low-dimensional (n = 3) for ease of interpretation by a reader. As shown in the following, convergence rates for such examples and for examples of higher dimension are the same.

6.1. Problem (P1). Example 1

In this example we calculate the point of time at which the reachable set \mathcal{R} first intersects the target set \mathcal{M} .

Consider the system

$$\dot{x} = Ax + Bu, \quad x(0) = 0, \quad u \in \mathbb{R}: \quad |u| \le 1, \quad A = \begin{bmatrix} -1.3 & 1 & 0\\ 0 & -1.3 & 1\\ 0 & 0 & -1.3 \end{bmatrix}, \quad B = \begin{bmatrix} 0\\ 0\\ 1 \end{bmatrix}.$$
 (23)

The target set is $\mathcal{M} = \mathcal{M}_0 + B_r(0)$, where \mathcal{M}_0 is the ball $B_{0,2}(0.7, -0.3, 0.35)$, r = 0.5. Recall that f(p) in problem (11) depends on t, i.e. $f(p,t) = s(p,\mathcal{R}(t)) + s(p,-\mathcal{M}_0)$.

We first consider the auxiliary problem of finding the distance between sets $\mathcal{R}(t)$ and \mathcal{M} for t = 1, with initial condition $p_1 = (0,03123620, -0.72453809, 0.68852659), f(p_1,1) = -0.05270947.$

Figure 2,a: Convergence of the gradient projection algorithm for the auxiliary problem $\min_{\|p\|=1} f(p,t)$ for t = 1. Approximation of the convergence rate is $f(p_k, 1) - f(p_0, 1) \approx 0.2486 \times 0.83043^k$. The found solution is $p_0 = (0.87540058, -0.46926876, 0.11602002)$ with $f(p_0, 1) = -0.573989$.

The reachable set and the point closest to the target set are depicted on Fig. 3.

When searching for the minimal time at which intersection occurs, we only know the search interval [0, T], but not the starting point p_1 for arbitrary moment of time from the interval. There are two different strategies. The first one is to randomly find $p_1 \in S_1$ with $f(p_1, t) < 0$ for a given t and increase t by a small amount. However, due to the time-related nature of (P1) there is a better algorithm. This algorithm involves keeping track of suitable p, f(p, t) < 0, while increasing the time.



Fig. 2. Convergence of gradient projection algorithm with step size $\lambda = 0.1$. (a) Problem (P1), Example 1, (b) problem (P1), Example 2.



Fig. 3. The point of the reachable set $\mathcal{R}(t)$ (t = 1) closest to the target set found by gradient projection algorithm (problem (P1), Example 1).

Algorithm for problem (P1) (finding minimal time)

Data: T > 0, f(p,t), r > 0, tolerance $\varepsilon_{tol} > 0$, bounds $t_{lower} = 0$, $t_{upper} = T$, time step $\Delta_t > 0$.

- (1) Put $t \leftarrow 0$ and find initial p_1 satisfying $f(p_1, 0) < 0$ first. Then run the gradient projection method which gives $p(0) = \arg \min_{\|p\|=1} f(p, 0) : f(p(0), 0) < 0$.
- (2) Put $t_{\text{test}} = \min\{t + \Delta_t, t_{\text{upper}}\}$. If $f(p(t), t_{\text{test}}) \ge 0$, then set $\Delta_t \leftarrow \Delta_t/2$ and repeat this step. If $f(p(t), t_{\text{test}}) < 0$, then proceed to Step (3).
- (3) Run the gradient projection method (13) for function $f(p, t_{\text{test}})$ with initial point $p_1 = p(t)$. It results in p_0 and $J = f(p_0, t_{\text{test}}) = \min_{\|p\|=1} f(p, t_{\text{test}}) < 0$.
- (4) If $J > -r + \varepsilon_{\text{tol}}$, then the reachable set intersects the set \mathcal{M} . Update $t_{\text{upper}} \leftarrow t_{\text{test}}$, $\Delta_t \leftarrow \frac{1}{2}\min\{\Delta_t, t_{\text{upper}} t_{\text{lower}}\}$ and proceed to Step (2) with the same t and p(t). Otherwise continue with Step (5).
- (5) If $J < -r \varepsilon_{\text{tol}}$, then the reachable set has yet to reach the set \mathcal{M} . Update $t_{\text{lower}} \leftarrow t_{\text{test}}$, $\Delta_t \leftarrow \min\{2\Delta_t, \frac{t_{\text{upper}} - t_{\text{lower}}}{2}\}$. Also update $t \leftarrow t_{\text{test}}, p(t) \leftarrow p_0$ and continue with Step (2). Otherwise finish with Step (6).
- (6) A solution is found within given tolerance: $|J + r| \leq \varepsilon_{\text{tol}}$. Return $t_0 = t_{\text{test}}$ as the optimal time for problem (P1), and p_0 .

Notes: the algorithm performs bisection-like search on the time interval [0, T]. Probability of finding suitable p_1 at Step (1) may be estimated using results from Section 5. However, it can be found non-randomly at Step (1) if we can somehow find a unit separation vector $p_1 \in \mathbb{R}^n$ such that $(p_1, x) \leq 0$ for all $x \in -\mathcal{M}_0$. Further at each Step (2), the initial value p_1 of the gradient projection algorithm is chosen non-randomly. At Step (5), the time step is doubled for faster search. The algorithm may also operate if the value T is unknown (i.e. $t_{upper} = \infty$), but for $t_{upper} > T$ convergence conditions for the gradient projection algorithm may be violated. Nevertheless the invariance $t_{lower} \leq t_{test} \leq t_{upper}$ is satisfied.

The algorithm stops when we obtain J with a given tolerance ε_{tol} , in all examples here and below $\varepsilon_{\text{tol}} = 10^{-7}$ and at the final stage $t_{\text{upper}} - t_{\text{lower}} \sim 10^{-6}$. We also can stop the algorithm with a given precision with respect to the time t: e.g. when $t_{\text{upper}} - t_{\text{lower}} \leq \varepsilon_{time}$ we finish calculations and take $t \in [t_{\text{lower}}, t_{\text{upper}}]$. Here $\varepsilon_{time} > 0$ is an admissible time error.

For system (23) Algorithm converges in 21 steps. The optimal time is 2.7383842,

 $p_0 = (0.77091811, -0.60777697, 0.19050571).$



Fig. 4. Attainable set at the moment of intersection and the optimal trajectory (problem (P1), Example 1).

Figure 4 depicts the reachable set and the target set at the moment when they intersect. The optimal trajectory (as in 9) with two switches can also be seen. Also see [24].

As was shown in Introduction, the reachable set $\mathcal{R}(t)$ of system (23) is not strongly convex. For $\mathcal{U} = B \times [-1, 1]$ and t > 0 we have $s(p, \mathcal{R}(t)) = \int_0^t e^{-1.3s} |p_1 \frac{s^2}{2} + p_2 s + p_3| \, ds$ for any $p = (p_1, p_2, p_3) \in \mathcal{S}_1$. For the solution $p_0 = (0.77091811, -0.60777697, 0.19050571)$ and t = 2.73838... we have the roots $s_1(p_0) < s_2(p_0)$ of the equation $p_1 \frac{s^2}{2} + p_2 s + p_3 = 0$ for $p = p_0$. By the inverse function theorem the roots $\mathcal{S}_1 \ni p \to s_i(p), i = 1, 2$, of the equation $p_1 \frac{s^2}{2} + p_2 s + p_3 = 0$ are analytic in some neighbourhood of the point $p_0 \in \mathcal{S}_1$. In other words, there exists a number $\gamma > 0$ such that the functions

$$\mathcal{S}_1 \cap B_\gamma(p_0) \ni p \to s_i(p), \quad i = 1, 2,$$

are Lipschitz continuous with some constant L > 0. Moreover, we can choose the number $\gamma > 0$ so that the first components of p and q are strictly positive and $\max\{s_1(p), s_1(q)\} \leq \min\{s_2(p), s_2(q)\}$ for all $p, q \in S_1 \cap B_{\gamma}(p_0)$.

Fix a pair of points $p, q \in S_1 \cap B_{\gamma}(p_0)$. Put $M = \max_{s \in [0,t]} \|e^{As}\|$. Then $|s_i(p) - s_i(q)| \leq L \|p - q\|$ for i = 1, 2 and for the supporting elements, using the estimate $\|\mathcal{U}(e^{A^Ts}p) - \mathcal{U}(e^{A^Ts}q)\| \leq 2$, we have

$$\|\mathcal{R}(t)(p) - \mathcal{R}(t)(q)\| = \sum_{i=1}^{2} \left\| \int_{s_i(p)}^{s_i(q)} e^{As} (\mathcal{U}(e^{A^T s} p) - \mathcal{U}(e^{A^T s} q)) \, ds \right\| \leq 4ML \|p - q\|.$$

Thus the part of surface $\{\mathcal{R}(t)(p) : p \in S_1 \cap B_\gamma(p_0)\}$ is a part of a strongly convex set with radius R = 4ML. In the present example it's enough for convergence of the gradient projection algorithm at time t. The same situation takes place for a time less than t.

6.2. Problem (P1), Example 2

Consider an example in \mathbb{R}^{12} .

 $A = \text{diag}(-0.3, -0.8, -1, -0.7, -0.71, -0.52, -0.37, -0.05, -0.25, -0.89, -0.99, -0.2), \ \mathcal{U} = B_1(0).$ The target set is $\mathcal{M} = \mathcal{M}_0 + B_r(0)$, where \mathcal{M}_0 is the ball $B_{0.4}(0.3 \times \mathbf{1})$ $(\mathbf{1} = (1, 1, \dots, 1)), r = 0.2$, step-size $\lambda = 0.1$.



Fig. 5. The kth components u_k of the optimal control (problem (P1), Example 2).

Figure 2,b: convergence of the gradient projection algorithm for the auxiliary problem $\min_{\|p\|=1} f(p,t)$ for the time t = 0.5 and the initial condition

 $p_1 = (0.02046203, 0.24278712, 0.2199823, 0.33539534, 0.11750331, 0.07584814, 0.44196329, 0.14159412, 0.08314335, 0.32560626, 0.49401057, 0.43339861)$

with $f(p_1, 0.5) = -0.047713028083805786$.

Approximation of convergence rate is $f(p_k, 0.5) - f(p_0, 0.5) \approx 0.1218 \times 0.8122^k$. The optimal value is

 $p_0 = (0.2730037, \ 0.30197686, \ 0.3125336, \ 0.29647251, \ 0.29702965, \ 0.28619273, \\ 0.27727228, \ 0.2572461, \ 0.26991497, \ 0.30680235, \ 0.31202019, \ 0.26679398)$

with $f(p_0, 0.5) = -0.2023841828091369$.

Algorithm converges in 21 steps to the point

 $p_0 = (0.27281666, 0.3021221, 0.31280135, 0.29655398, 0.29711758, 0.28615572, 0.27713348, 0.25688441, 0.26969324, 0.30700357, 0.31228196, 0.26653741)$

and the optimal time is 0.503150463104248.

Figure 5 illustrates the optimal control (per components, each line means one of 12 components).

6.3. Problem (P2). Example 3

The reachable set (as in (23)) is touching the target set from the inside. The target set is the ellipsoid $\mathcal{M} = \{x : (x-c)^T Q(x-c) \leq R^2\}$, with

$$Q = \begin{bmatrix} 4.5 & -1.2 & -1.6 \\ -1.2 & 6.8 & -2.3 \\ -1.6 & -2.3 & 8 \end{bmatrix}, \quad c = \begin{bmatrix} -3.4 \\ -3.8 \\ 0.3 \end{bmatrix}, \quad R = 12.$$

Recall that $f(p,t) = s(p,\mathcal{M}) - s(p,\mathcal{R}_{\varepsilon}(t))$, here we take $\varepsilon = 0.05$, step-size $\lambda = 0.2$.



Fig. 6. Solution of problem (P2), Example 3.

Figure 6: For system (23) a similar bisection algorithm converges in 19 steps (i.e. $|J + \varepsilon| \leq \varepsilon_{\text{tol}} = 10^{-7}$). The optimal time is t = 1,64610733, $p_0 = (0,36800454, 0,72705740 - 0,57962073)$.

6.4. Problem (P2). Example 4. Homothete Inside the Target Set

We solve problem (P2) for a homothete, i.e. the problem is stated as

$$\max_{t \ge 0} t : \quad t\mathcal{R} \subset \mathcal{M}.$$
⁽²⁴⁾

Define $\mathcal{M} = B_{10}(0)$, i.e. the ball centered at 0 of radius 10. The set \mathcal{R} is a strongly convex segment with endpoints [-0.1, 3, 2.05884573], [-1.9, 3, -1.05884573] and radius of strong convexity R = 3, i.e. \mathcal{R} is the intersection of all closed balls of radius R = 3 containing the endpoints.

The supporting element for a unit vector $p = (p_1, \ldots, p_n)$ for a strongly convex segment with endpoints $[-ae_1, ae_1]$ and radius of strong convexity R > a is equal to $Rp - \frac{\sqrt{R^2 - a^2}}{\sqrt{1 - p_1^2}}(I - e_1e_1^T)p$ if $\arctan(\frac{p_1}{\sqrt{1 - p_1^2}}) < \arctan(\frac{a}{R})$, otherwise it is equal to $\operatorname{sign}(p_1)ae_1$. We shall consider the homothety $t\mathcal{R}$, with parameter $\varepsilon = 0.1$ in the definition of f in (15), and step-size $\lambda = 0.2$.



Fig. 7. Problem (P2), Example 4. The homothete is not contained inside \mathcal{M} when t = 3.

For t = 3 the set $t\mathcal{R}$ is not contained in \mathcal{M} (see Fig. 7). An algorithm, similar to one for problem (P2), in 21 steps gives the optimal value $t_0 = 2.62904820$ and $p_0 = (-0.3425777, 0.93398621, 0.10153957)$ (i.e. $|J + \varepsilon| \leq \varepsilon_{\text{tol}} = 10^{-7}$).

6.5. Problem (P3). Example 5

Consider an example in \mathbb{R}^{10}

 $A = \text{diag}(0.1, 0.75, 0.8, 0.81, 0.82, 0.95, 1.0, 1.0, 1.05, 1.1), \quad \mathcal{U} = B_1(0). \quad \text{The target set is } \mathcal{M} = B_{0.1}(0.1 \times \mathbf{1}), \ (\mathbf{1} = (1, 1, \dots, 1)), \ \varepsilon = 0.1, \text{ step-size } \lambda = 0.1.$

We need 21 runs of the gradient projection algorithm to get the solution point

 $p_0 = (0.44643102, 0.32328081, 0.3153902, 0.3138356, 0.31228874,$

0.29286442, 0.28572048, 0.28572048, 0.27875066, 0.27195027)

and the optimal time is $t_0 = 0.35823087$.

7. CONCLUSION

In this paper we used a minimization Problem 1 to propose effective solution methods for several other problems (P1)—(P3) that involve distances and inclusions between sets. Linear convergence of proposed algorithms is proven. Several examples are given to prove the effectiveness of proposed solutions.

APPENDIX

A.1. PROOF OF LEMMA 1

Multiply both sides of the inequality by $\sqrt{\|p\| \|q\|}$ and take the square.

A.2. PROOF OF LEMMA 3

By the equality $e^{As} = Je^{A_1s}J^{-1}$ we get

$$\mathcal{R}(t) = \int_{0}^{t} J e^{A_1 s} J^{-1} \mathcal{U} \, ds = \int_{0}^{t} J e^{A_1 s} \mathcal{U}_1 \, ds = J \mathcal{R}_1(t).$$

The result follows from [25, Theorem 3].

A.3. PROOF OF LEMMA 3

We have $\mathcal{U} = \mathcal{U}_0 + \mathcal{B}_r(0)$. Then $\mathcal{R}(t) = \mathcal{R}_0(t) + r \int_0^t e^{As} \mathcal{B}_1(0) ds$,

$$\mathcal{R}_0(t) = \int\limits_0^t e^{As} \mathcal{U}_0 \, ds$$

It is enough to prove that the ellipsoid $e^{As}\mathcal{B}_1(0)$ is uniformly smooth with constant $r(s) = \frac{\lambda_n^2(s)}{\lambda_1(s)}$. Consider orthonormal basis where the ellipsoid $e^{As}\mathcal{B}_1(0)$ has a canonical form

$$\mathcal{N} = \left\{ x \in \mathbb{R}^n : \sum_{k=1}^n \frac{x_k^2}{\lambda_k^2} \leqslant 1 \right\}, \quad \lambda_k = \lambda_k(s).$$

Then the matrix $L = \text{diag} \{\lambda_1, \ldots, \lambda_n\}$ gives $L\mathcal{B}_1(0) = \mathcal{N}$. The ellipsoid $\mathcal{V} = \{x : \sum_{k=1}^n \lambda_k^2 x_k^2 \leq 1\}$ is strongly convex with radius $\rho = \lambda_1 / \lambda_n^2$. Hence there exists another compact convex set \mathcal{P} with $\mathcal{V} + \mathcal{P} = \mathcal{B}_{\rho}(0)$ and, taking in mind that $L\mathcal{V} = \mathcal{B}_1(0)$, we have

$$L\mathcal{V} + L\mathcal{P} = L\mathcal{B}_{\rho}(0) = \rho L\mathcal{B}_{1}(0) = \rho \mathcal{N} \quad \Leftrightarrow \quad \frac{1}{\rho}\mathcal{B}_{1}(0) + \frac{1}{\rho}\mathcal{P} = \mathcal{N}.$$

Thus the set \mathcal{N} is uniformly smooth with constant $\frac{1}{\rho} = \lambda_n^2 / \lambda_1$.

BALASHOV et al.

A.4. PROOF OF THEOREM 1

Let I be the identity matrix. Assume that $p_0 \in S_1$ is the solution of problem (1). From the necessary condition of extremum $f(p_0) = (p_0, f'(p_0)) = -\|f'(p_0)\|$. Then $P_{\mathcal{T}_p} = I - pp^T$ for any $p \in S_1$ and $\|(I - pp^T)f'(p)\|^2 = \|f'(p)\|^2 - f^2(p)$. Hence for all $p \in S$ we get

$$||f'(p)||^2 - f^2(p) = (||f'(p)|| - f(p))(||f'(p)|| + f(p_0) + f(p) - f(p_0)).$$

From the inequality $f(p) \leq 0$ and the fact that the supporting element $f'(p_0) = \mathcal{N}(t)(p_0)$ has minimal norm, we have $||f'(p)|| - f(p) \geq ||f'(p)|| \geq ||f'(p_0)|| = |J|$. It remains to note that $||f'(p)|| + f(p_0) = ||f'(p)|| - ||f'(p_0)|| \geq 0$.

For any vectors $p, q \in \mathbb{R}^n$, $1 - \varepsilon \leq ||p||$, $||q|| \leq 1 + \varepsilon$, by Lemma 1 we obtain that $\left\|\frac{p}{||p||} - \frac{q}{||q||}\right\| \leq \frac{||p-q||}{\sqrt{||p|| ||q||}}$. Fix such p, q. Then by Lipschitz continuity of the supporting element $f'(\xi) = \mathcal{N}(t)(\xi)$ on the unit sphere with Lipschitz constant R and by the equality $f'(\xi) = f'(\xi/||\xi||)$, for all $\xi \neq 0$, we get

$$\|f'(p) - f'(q)\| \leq R \left\|\frac{p}{\|p\|} - \frac{q}{\|q\|}\right\| \leq \frac{R\|p - q\|}{\sqrt{\|p\|\|q\|}} \leq \frac{R}{1 - \varepsilon}\|p - q\|. \quad \Box$$

A.5. PROOF OF THEOREM 2

Define $q_k = p_k - \lambda f'(p_k)$, $||q_k|| \ge 1 - \lambda ||f'(p_k)|| \ge 1 - \lambda L \ge \frac{1}{2}$. By $||p_k|| = ||p_{k+1}|| = 1$, Lemma 1 and from the inequality

$$\|p_{k+1} - p_k\| = \|P_{\mathcal{S}_1}(p_k - \lambda f'(p_k)) - p_k\| \leq \frac{\|p_k - q_k\|}{\sqrt{\|p_k\| \|q_k\|}} \leq \lambda \sqrt{2} \|f'(p_k)\| \leq \lambda \sqrt{2}L \leq \frac{1}{\sqrt{2}}$$

we get $[p_k, p_{k+1}] \subset \{p \in \mathbb{R}^n : \frac{1}{2} \leq ||p|| \leq \frac{3}{2}\}$. By Theorem 1 f' is Lipschitz continuous on the segment $[p_k, p_{k+1}]$ with constant $L_1 = R/(1 - \frac{1}{2}) = 2R$.

We also have the LPL condition for the function f on the set S by Theorem 1 with $\mu = |J|$.

Fix λ from the proposition and $\ell = \frac{1}{\lambda} \ge L_1$. Put $z_k = \|\ell p_k - f'(p_k)\| - (p_k, p_k - f'(p_k)) \ge 0$,

$$z_{k} = \frac{\|(I - p_{k}p_{k}^{T})f'(p_{k})\|^{2}}{\|\ell p_{k} - f'(p_{k})\| + (p_{k}, p_{k} - f'(p_{k}))} \ge \frac{\|(I - p_{k}p_{k}^{T})f'(p_{k})\|^{2}}{2\|\ell p_{k} - f'(p_{k})\|}.$$
(A.1)

We have

$$||p_{k+1} - p_k||^2 = 2 - 2\frac{(p_k, \ell p_k - f'(p_k))}{\|\ell p_k - f'(p_k)\|} = \frac{2z_k}{\|\ell p_k - f'(p_k)\|}$$

and from the Lipschitz property of f' on the segment $[p_k, p_{k+1}]$ with constant L_1

$$f(p_{k+1}) - f(p_k) \leq (f'(p_k), p_{k+1} - p_k) + \frac{L_1}{2} \|p_{k+1} - p_k\|^2$$

= $(p_k, L_1 p_k - f'(p_k)) - \left(L_1 p_k - f'(p_k), \frac{\ell p_k - f'(p_k)}{\|\ell p_k - f'(p_k)\|}\right)$
= $\left(\ell p_k - f'(p_k) + (L_1 - \ell)p_k, p_k - \frac{\ell p_k - f'(p_k)}{\|\ell p_k - f'(p_k)\|}\right)$,
 $f(p_{k+1}) - f(p_k) \leq -z_k + (L_1 - \ell)\left(p_k, p_k - \frac{\ell p_k - f'(p_k)}{\|\ell p_k - f'(p_k)\|}\right) = -z_k + \frac{L_1 - \ell}{\|\ell p_k - f'(p_k)\|}z_k \leq -z_k$.

From (A.1) and from the LPL condition with $\mu = |J|$ we obtain that

$$f(p_{k+1}) - f(p_k) \leqslant -\frac{\|(I - p_k p_k^T) f'(p_k)\|^2}{2\|\ell p_k - f'(p_k)\|} \leqslant -\frac{|J|}{2\|\ell p_k - f'(p_k)\|} (f(p_k) - f(p_0)).$$

AUTOMATION AND REMOTE CONTROL Vol. 85 No. 5 2024

Define $\varphi(p) = f(p) - f(p_0)$ for all $p \in S_1$. From the estimate $||\ell p_k - f'(p_k)|| \leq \ell + ||f'(p_k)|| \leq \ell + L$ we have

$$\varphi(p_{k+1}) \leqslant \left(1 - \frac{|J|}{2\ell + 2L}\right)\varphi(p_k) = q\varphi(p_k)$$

and $q \in (0,1)$ because $|J| = \rho(0, \mathcal{N}(t)) \leq ||\mathcal{N}(t)|| = L$.

For the points $\{p_k\}$ we have (note that $||p_k - \lambda f'(p_k)|| \ge 1$)

$$\|p_{k+1} - p_k\|^2 \leq \frac{2z_k}{\|\ell p_k - f'(p_k)\|} \leq \frac{2\lambda(f(p_k) - f(p_{k+1}))}{\|p_k - \lambda f'(p_k)\|} \leq 2\lambda\varphi(p_k).$$

A.6. PROOF OF THEOREM 3

Consider f(p):

$$f(p) = s(p, \mathcal{M}_0) + r \|p\| - s(p, \mathcal{R}_{\varepsilon}(t)).$$

The set $\mathcal{R}_{\varepsilon}(t)$ is strongly convex with radius $R_T + \varepsilon < r$. Hence there exists another convex compact set $\mathcal{N}(t)$ with $\mathcal{R}_{\varepsilon}(t) + \mathcal{N}(t) = \mathcal{B}_{R_T + \varepsilon}(0)$ and $r \|p\| - s(p, \mathcal{R}_{\varepsilon}(t)) = (r - R_T - \varepsilon) \|p\| + s(p, \mathcal{N}(t))$. Thus for all $p \in \mathbb{R}^n$

$$f(p) = s(p, \mathcal{M}_0) + (r - R_T - \varepsilon) \|p\| + s(p, \mathcal{N}(t)) = s(p, \mathcal{M}_0 + \mathcal{N}(t) + \mathcal{B}_{r - R_T - \varepsilon}(0))$$

and the function f(p) is the supporting function of the set $\mathcal{N}(t) = \mathcal{M} \stackrel{*}{=} \mathcal{R}_{\varepsilon}(t) = \mathcal{M}_0 + \mathcal{N}(t) + \mathcal{B}_{r-R_T-\varepsilon}(0)$. The latter set is strongly convex with radius R_0 and uniformly smooth with constant $r_0 = r - R_T - \varepsilon > 0$. The function f' is Lipschitz on the set \mathcal{S}_1 with constant R_0 and as in the proof of Proposition 2 $[p_k, p_{k+1}] \subset \{p \in \mathbb{R}^n : \frac{1}{2} \leq \|p\| \leq \frac{3}{2}\}$. Thus for any point p from the segment $[p_k, p_{k+1}]$ we have $\|p\| \ge \frac{1}{2}$ and for any $p, q \in [p_k, p_{k+1}]$ by Lemma 1

$$\|f'(p) - f'(q)\| = \left\|f'\left(\frac{p}{\|p\|}\right) - f'\left(\frac{q}{\|q\|}\right)\right\| \le R_0 \left\|\frac{p}{\|p\|} - \frac{q}{\|q\|}\right\| \le R_0 \frac{\|p - q\|}{\sqrt{\|p\| \|q\|}} \le 2R_0 \|p - q\|,$$

i.e. f' is Lipschitz on any segment $[p_k, p_{k+1}]$ with constant $2R_0$. From the Lipschitz property of f' and Proposition 2 $f(p_k) \leq 0$ for all k.

$$||p_{k+1} - p_0||^2 = ||P_{\mathcal{S}_1}(p_k - \lambda f'(p_k)) - P_{\mathcal{S}_1}(p_0 - \lambda f'(p_0))||^2,$$

 $||p_k - \lambda f'(p_k)|| \ge 1$, $||p_0 - \lambda f'(p_0)|| \ge 1$, i.e. $p_k - \lambda f'(p_k) \notin \text{int } B_1(0)$, $p_0 - \lambda f'(p_0) \notin \text{int } B_1(0)$ and thence

$$||p_{k+1} - p_0||^2 \leq ||p_k - p_0 + \lambda (f'(p_k) - f'(p_0))||^2$$

$$\leq ||p_k - p_0||^2 - 2\lambda (p_k - p_0, f'(p_k) - f'(p_0)) + \lambda^2 ||f'(p_k) - f'(p_0)||.$$

From the strong convexity of the set $\mathcal{N}(t)$ with radius R_0 we have $||f'(p_k) - f'(p_0)|| \leq R_0 ||p_k - p_0||$. Also by the strong convexity of the set $\mathcal{N}(t)$ with radius R_0 we have [28, Theorem 2.1 (h)] $(p_k - p_0, f'(p_k) - f'(p_0)) \geq \frac{1}{R_0} ||f'(p_k) - f'(p_0)||^2$ and by the uniform smoothness of the set $\mathcal{N}(t)$ with constant r_0 [28, Definition 3.2, Theorem 3.6]

$$(p_k - p_0, f'(p_k) - f'(p_0)) \ge \frac{1}{R_0} \|f'(p_k) - f'(p_0)\|^2 \ge \frac{r_0^2}{R_0} \|p_k - p_0\|^2.$$

Thus $||p_{k+1} - p_0||^2 \leq q^2 ||p_k - p_0||^2$.

BALASHOV et al.

A.7. PROOF OF THEOREM 4

Repeat the proof of Theorem 3. In particular, the function f(p) is the supporting function for the set $\mathcal{R}(t) \stackrel{*}{\longrightarrow} \mathcal{M}_{\varepsilon} = \mathcal{R}(t) \stackrel{*}{\longrightarrow} \mathcal{M}_{\varepsilon}^{*} \mathcal{B}_{\varepsilon}(0)$. The last set is strongly convex with constant R_T and uniformly smooth with constant r.

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TOPICAL ISSUE

Approximation-Based Approach to Adaptive Control of Linear Time-Varying Systems

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Abstract—An adaptive state-feedback control system is proposed for a class of linear timevarying systems represented in the controller canonical form. The adaptation problem is reduced to the one of Taylor series-based first approximations of the ideal controller parameters. The exponential convergence of identification and tracking errors of such an approximation to an arbitrarily small and adjustable neighbourhood of the equilibrium point is ensured if the condition of the regressor persistent excitation with a sufficiently small time period is satisfied. The obtained theoretical results are validated via numerical experiments.

Keywords: adaptive control, time-varying parameters, parametric error, persistent excitation, identification

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1. INTRODUCTION

Starting from the 1960s, the subject of adaptive control has been one of the central ones for Laboratory No. 7 of V.A. Trapeznikov Institute of Control Sciences of RAS. Its founder, academician Yakov Zalmanovich Tsypkin, made a significant contribution to research on adaptation and learning problems and proposed a unified approach to their solution based on stochastic approximation methods. Using it, in particular, the problems of identification and parameter estimation were successfully solved. Subsequently, Boris Theodorovich Polyak proposed optimal and robust pseudogradient adaptation algorithms and strictly analysed their convergence rate [1, 2]. These studies have largely become the foundations of the adaptive control theory, which, having started with linear systems with time-invariant parameters, is gradually being generalised to wider classes of plants. One such class will be discussed in this study.

One of the subjects of adaptive control theory is the problem of the time-invariant reference model tracking by a time-varying plant with zero steady-state error. Despite more than 65 years of efforts, this problem still lacks a universal practical solution, which motivates researchers all over the world to design new approaches and tools.

Conventional adaptive control algorithms are applicable to linear systems with quasi-timeinvariant parameters. When they are applied to control linear time-varying systems, an uncompensated summand occurs in the derivative of the Lyapunov function, which is proportional to the rate of the unknown parameters change. As a result, instead of the convergence of the tracking error to zero, only its boundedness inside some ball with non-adjustable boundary is guaranteed. In [4], based on the speed-gradient method, these results are generalised to the problem of a timevarying reference model tracking by a nonlinear time-varying system. In [5, 6], various composite adaptive laws are proposed, which are claimed to reduce the steady-state error value in case the regressor persistent excitation condition is met. In [7], a congelation of variables method is proposed, which allows one to damp the above-mentioned uncompensated summand with the help of not always suitable for practice high-gain feedback, thus ensuring asymptotic convergence of the tracking error to zero. The alternative approach [8] also provides asymptotic stability, but uses a high gain in the adaptive law instead of the control one. Considering the method of majorizing functions [9, 10], the high gain is also used in the adaptive law, but, in contrast to [8], only dissipativity of the closed-loop system is guaranteed. In [11] an adaptive control system is proposed that provides exponential convergence of the tracking error to zero for systems represented in the controllable canonical form with time-varying parameters that are described by known exosystems with unknown initial conditions. In [12] it is proposed to reduce the problem of adaptive control of time-varying mechanical systems to the identification of the piecewise-constant parameters of the polynomial obtained by local expansion of the system time-varying parameters into a Taylor series of an arbitrary order. In [13, 14], based on the parametric identification methods, an approach to adaptive-optimal output feedback control of time-varying functions of time.

The disadvantages of the described above and other known approaches to solve the time-varying system adaptive control problems can be classified as follows:

- 1) application of high-gain in the control or adaptive law (sliding-mode control, high values of the parameters, nonlinear damping signals, etc.) [7–10, 12];
- 2) the necessity to meet the parametric identifiability conditions [5, 6, 11, 13, 14];
- 3) the dimensionality of the identification/adaptation problem to be solved is enlarged by taking into account the coefficients of the physical laws of the system parameters change or approximation polynomials [11–14].

A more complete state-of-the-art understanding of the time-varying systems adaptive control problem can be obtained from the statement sections of the cited studies [4–15]. In this paper, a new approximation-based adaptive control method, which exploits the parameter identification theory, is proposed for time-varying systems.

The motivation is to investigate the applicability conditions of the recently proposed algorithm [16] that identifies time-varying parameters of a linear regression equation to solve the time-varying linear system control problem. According to [16], the problem of time-varying parameters identification is reduced to the one of estimation of their piecewise-constant approximation. As follows from the theoretical conclusions of [16], unlike many existing methods of time-varying parameters identification, the algorithm from [16] allows one to ensure convergence of the timevarying parameters identification error to a region, which can be arbitrarily reduced by decreasing the Taylor series expansion time interval in case the regressor is persistently exciting over a sufficiently small period of excitation T_s . In this study, the approach is proposed to be used to control a class of linear systems with time-varying parameters. To that end:

- 1) a non-adaptive control law is proposed for a time-varying system, which feedback and forward parameters are calculated only via the first (piecewise-constant) approximation of the system time-varying parameters;
- 2) in case the control law from 1) is applied, the convergence conditions of the tracking error to an arbitrarily small neighbourhood of zero are obtained;
- 3) based on the results from [16], the law to estimate the parameters of the controller from 1) is proposed, which allows one to ensure the convergence of the tracking error to an arbitrarily small neighbourhood of zero in case the regressor is persistently exciting with a sufficiently small period of excitation.

Considering the above-given literature review, the obtained approximation-based approach to design adaptive control systems for time-varying plants is close to [12]. However, unlike in [12],

firstly, the time-varying parameters are approximated only by the first summand of Taylor series, which reduces the computational complexity and does not increase the dimensionality of the identification problem, and secondly, the step of the obtained estimates interpolation is not needed. In comparison with other existing solutions [4-14], the proposed algorithm of adaptive control of time-varying linear systems has the following advantages (+) and disadvantages (-):

- (+) high gain and damping components are not used in both control and adaptive laws;
- (+) the function of the time-varying parameters change is not required to be known;
- (+) no *a priori* information about the system parameters is used;
- (-) the repressor persistent excitation condition is required to be met to achieve even asymptotic convergence of the tracking error to a neighbourhood of zero;
- (-) the value of the steady-state tracking error can be reduced only if the period T_s of the regressor persistent excitation is small enough;
- (-) violation of the parametric identifiability condition (the regressor persistent excitation) may result in instability of the closed-loop system.

In general, although the proposed solution does not overcome all the shortcomings of the existing approaches, it expands the set of adaptive control methods for the time-varying systems, and therefore, in the authors' opinion, it is of interest.

Notation and Definitions

The following notation is adpoted: $f(t) \in \mathbb{R}^{n \times m}$ means a value of a function $f: [t_0^+, +\infty) \to \mathbb{R}^{n \times m}$ at the time point t, where $t_0^+ \ge 0$ is an initial time instant; for a vector $a \in \mathbb{R}^n$ the notation ||a|| is the Euclidean norm; the minimum and maximum eigenvalues of a matrix $A \in \mathbb{R}^{n \times n}$ are denoted as $\lambda_{\min}(A)$ and $\lambda_{\max}(A)$, respectively. The abbreviation exp stands for the exponential stability.

The definitions of finite and persistent excitation are used to prove theorems and propositions.

Definition 1. A signal $\omega(t) \in \mathbb{R}^n$ is finitely exciting over a time range $[t_1, t_2] \subset [t_0^+, \infty)$ if there exists $\alpha > 0$ such that the following inequality holds:

$$\int_{t_1}^{t_2} \omega(\tau) \,\omega^{\mathrm{T}}(\tau) \,d\tau \ge \alpha I_n.$$
(1.1)

Definition 2. A signal $\omega(t) \in \mathbb{R}^n$ is persistently exciting if for all $t \ge t_0^+ \ge 0$ there exist $T_s > 0$ and $\alpha > 0$ such that the following inequality holds:

$$\int_{t}^{t+T_{s}} \omega(\tau) \,\omega^{\mathrm{T}}(\tau) \,d\tau \ge \alpha I_{n}.$$
(1.2)

Set of signals, for which condition (1.1) or (1.2) is met, we denote as FE or PE, respectively. A signal $\omega(t)$ is persistently exciting if $\omega \in \text{PE}$, and it is finitely exciting if $\omega \in \text{FE}$.

The main result of the study utilises the Taylor formula with integral remainder. The conditions of existence of such equation are defined in the following lemma [17].

Lemma 1. Let (t_1, t_2) be an open time interval, and $f(t) \in \mathbb{R}$ be a p-times continuously differentiable function of time t, then for any pair of time instants t and a from (t_1, t_2) it holds that

$$f(t) = f(a) + \frac{t-a}{1!} f^{(1)}(a) + \ldots + \frac{(t-a)^p}{p!} f^{(p)}(a) + \int_a^t \frac{(t-\zeta)^p}{p!} f^{(p+1)}(\zeta) \, d\zeta.$$
(1.3)

2. PROBLEM STATEMENT

We consider continuous linear systems with time-varying parameters

$$\dot{x}(t) = A(t)x(t) + B(t)u(t) = A_0 x(t) + e_n \left(a^{\mathrm{T}}(t) x(t) + b(t) u(t) \right)$$

= $A_0 x(t) + e_n \Phi^{\mathrm{T}}(t) \Theta(t), \quad x \left(t_0^+ \right) = x_0,$ (2.1)

where

$$A(t) = A_0 + e_n a^{\mathrm{T}}(t), \quad B(t) = e_n b(t),$$
$$A_0 = \begin{bmatrix} 0_{(n-1)\times 1} & I_{n-1} \\ 0_{1\times n} \end{bmatrix}, \quad e_n = \begin{bmatrix} 0_{(n-1)\times 1} \\ 1 \end{bmatrix}, \quad \Theta(t) = \begin{bmatrix} a^{\mathrm{T}}(t) & u(t) \end{bmatrix},$$
$$\Theta(t) = \begin{bmatrix} a^{\mathrm{T}}(t) & b(t) \end{bmatrix}^{\mathrm{T}},$$

 $x(t) \in \mathbb{R}^n$ is a state vector with unknown initial conditions x_0 , $u(t) \in \mathbb{R}$ stands for a control signal, $A(t) \in \mathbb{R}^{n \times n}$ denotes an unknown matrix of the system under consideration, $B(t) \in \mathbb{R}^n$, $\Theta(t) \in \mathbb{R}^{n+1}$ are unknown vectors, $A_0 \in \mathbb{R}^{n \times n}$ stands for a Frobenius matrix, $e_n \in \mathbb{R}^n$ is the *n*th Euclidean basis vector. The pair (A(t), B(t)) is completely controllable for all $t \ge t_0^+$. The controllability condition for the system (2.1) can be validated via application of, for example, a criterion given in [18].

A salient feature of the class of systems (2.1) is the fact that control and uncertainty signals are in the same equation. Such systems are called the ones with matched uncertainty, and they are widely met in practice. For example, the Euler angles dynamics of a rigid body, assuming its symmetry, is described by a second-order system with matched uncertainty. Another good example of a control problem with matched uncertainties is the control of a manipulator state using the Euler–Lagrange formalism.

The following assumption is adopted with respect to the unknown parameters $\Theta(t)$.

Assumption 1. The parameters $\Theta(t)$ and their first and second derivatives are continuous and bounded

$$\|\Theta(t)\| \leq \Theta_{\max}, \|\dot{\Theta}(t)\| \leq \dot{\Theta}_{\max}, \|\ddot{\Theta}(t)\| \leq \ddot{\Theta}_{\max}$$

where the upper bounds Θ_{\max} , $\dot{\Theta}_{\max}$ and $\ddot{\Theta}_{\max}$ exist, but they are unknown.

The required control quality for the closed-loop system that includes the system (2.1) and the controller is defined with the help of the reference model with time-invariant parameters

$$\dot{x}_{ref}(t) = A_0 x_{ref}(t) + e_n \left(b_{ref} r(t) + a_{ref}^{\mathrm{T}} x_{ref}(t) \right), \ x_{ref} \left(t_0^+ \right) = x_{0ref},$$
(2.2)

where $x_{ref}(t) \in \mathbb{R}^n$ is a reference model state vector with known initial conditions x_{0ref} , $r(t) \in \mathbb{R}$ denotes a reference signal, $A_{ref} = A_0 + e_n a_{ref}^{\mathrm{T}} \in \mathbb{R}^{n \times n}$ stands for a Hurwitz reference model state matrix, b_{ref} is a reference model high frequency gain.

We assume that the reference model (2.2) is chosen in such a way that the matching conditions are met, *i.e* the state vector of (2.1) can ideally track the one of (2.2).

Assumption 2. There exist parameters $k_x(t) \in \mathbb{R}^{1 \times n}$ and $k_r(t) \in \mathbb{R}$ such that the following equations hold

$$a_{ref}^{T} - a^{T}(t) = b(t) k_{x}(t), \quad b_{ref} = b(t) k_{r}(t).$$

This assumption is necessary and sufficient condition for the existence of a control signal u(t) that ensures for all $t \ge t_0^+$ that the equations of the system (2.1) coincide with those of the chosen reference model (2.2). The assumption is ensured to be satisfied by choosing a reference model

in the form of (2.2), by consideration of a class of systems with a time-invariant sign of the highfrequency gain b(t) and by a completely controllable pair (A(t), B(t)). It should be noted that Assumption 2 imposes the following constraint on the system (2.1): sgn (b(t)) = const,¹ and hence jointly Assumptions 1 and 2 require boundedness of $b_{\max} \ge |b(t)| \ge b_{\min} > 0$.

The aim is to design an adaptive control law u(t), which, if $\Phi \in PE$, ensures exponential convergence (exp) of the error $e_{ref}(t) = x(t) - x_{ref}(t)$ into the goal set

$$\lim_{t \to \infty} \|e_{ref}(t)\| \leqslant \Delta_{e_{ref}}(\exp), \qquad (2.3)$$

in such a way that there exists some parameter of the adaptive control procedure, from which value the steady-state error $\Delta_{e_{ref}} > 0$ depends.

3. PRELIMINARY RESULTS AND TRANSFORMATIONS

An effective solution of the control problem of a linear system with unknown piecewise-constant parameters has been obtained recently in [19]. In this section the problem of adaptive control of a system (2.1) with time-varying parameters will be transformed into the one of control of a system with the piecewise-constant parameters. To this end, first of all, we show that the stated goal (2.3) is achievable with the help of the non-adaptive control law with known ideal parameters, which uses only piecewise-constant approximations of the time-varying parameters of the system (2.1) in its feedback and feedforward summands.

Taking into account Assumption 1, the error equation between the plant (2.1) and the reference model (2.2) is written as

$$\dot{e}_{ref}(t) = A_{ref}e_{ref}(t) + e_n b(t) [u(t) - k_x(t) x(t) - k_r(t) r(t)] = A_{ref}e_{ref}(t) + e_n b(t) [u(t) - \mathcal{K}^{\mathrm{T}}(t) \omega(t)],$$
(3.1)

where

$$e_{ref}(t) = x(t) - x_{ref}(t), \quad \omega(t) = \begin{bmatrix} x^{\mathrm{T}}(t) & r^{\mathrm{T}}(t) \end{bmatrix}^{\mathrm{T}} \in \mathbb{R}^{n+1},$$
$$\mathcal{K}(t) = \begin{bmatrix} k_x(t) & k_r(t) \end{bmatrix}^{\mathrm{T}} \in \mathbb{R}^{(n+1)\times 1}.$$

The disturbance $\mathcal{K}^{\mathrm{T}}(t) \omega(t)$ is going to be represented as a sum of two terms: with the piecewiseconstant and time-varying parameters. To that end, a growing sequence is introduced

$$t_i^+ = T \left\lfloor \frac{t - t_0^+}{T} \right\rfloor, \quad i \in \mathbb{N},$$

where $t_{i+1}^+ - t_i^+ = T > 0$, $\lfloor . \rfloor : \mathbb{R} \to \mathbb{Z}$ is a function to round down to the closest integer.

As, owing to Assumptions 1 and 2, the parameters $\mathcal{K}(t)$ are differentiable, then, following the Taylor equation (1.3), it can be written for the neighbourhood T of the time instant t_i^+ :

$$\mathcal{K}(t) = \mathcal{K}\left(t_{i}^{+}\right) + \int_{t_{i}^{+}}^{t} \dot{\mathcal{K}}(\zeta) d\zeta, \qquad (3.2)$$

where $\mathcal{K}(t_i^+) = \mathcal{K}_i$ are values of the parameters $\mathcal{K}(t)$ at the time instant t_i^+ , $\|\delta_{\mathcal{K}0}(t)\| \leq \dot{\mathcal{K}}_{\max}T$ is the reminder of the zeroth order (p = 0, see (1.3)).

¹ Otherwise there exists a time instant $t_a \ge t_0^+$ at which $b(t_a) = 0$, and equations from Assumption 2 have no solution in the general case $(b_{ref} \ne 0, a_{ref} - a(t_a) \ne 0_n)$.



Fig. 1. Graphical illustration of relationship between $\mathcal{K}(t)$, $\theta(t)$ and $\hat{\theta}(t)$.

Owing to (3.2), for each time range $[t_i^+, t_i^+ + T]$ the time-varying parameters $\mathcal{K}(t)$ can be approximated by their value \mathcal{K}_i at the beginning of such time range. Then the sequence of such values $\{\mathcal{K}_0, \mathcal{K}_1, \ldots, \mathcal{K}_i\}$ together with the sequence of the switching time instants $\{t_0^+, t_1^+, \ldots, t_i^+\}$ define the piecewise-constant signal, which is the first approximation of the time-varying parameters $\mathcal{K}(t)$ for all $t \ge t_0^+$:

$$\theta(t) = \mathcal{K}_i = \mathcal{K}_0 + \sum_{q=1}^i \Delta_q^{\theta} h\left(t - t_q^+\right), \tag{3.3}$$

where $\Delta_q^{\theta} = \mathcal{K}_q - \mathcal{K}_{q-1}$ is the amplitude of the parameters $\mathcal{K}(t)$ change over the time range $\left[t_i^+, t_{i+1}^+\right]$, $h: [t_0^+, \infty) \to \{0, 1\}$ stands for the Heaviside function.

For all $t \ge t_0^+$, equation (3.3) allows one to write the time-varying parameters as a sum $\mathcal{K}(t) = \theta(t) + \delta_{\mathcal{K}0}(t)$, which results in the required representation of the disturbance

$$\dot{e}_{ref}\left(t\right) = A_{ref}e_{ref}\left(t\right) + e_{n}b\left(t\right)\left[u\left(t\right) - \theta^{\mathrm{T}}\left(t\right)\omega\left(t\right) - \delta_{\mathcal{K}0}^{\mathrm{T}}\left(t\right)\omega\left(t\right)\right].$$
(3.4)

Equation (3.4) motivates to introduce the following implementable continuous non-adaptive control law

$$u(t) = \hat{\theta}^{\mathrm{T}}(t)\,\omega(t)\,, \qquad (3.5a)$$

$$\dot{\hat{\theta}}(t) = -\gamma_1 \left(\hat{\theta}(t) - \theta(t) \right) = -\gamma_1 \tilde{\theta}(t), \quad \hat{\theta}\left(t_0^+ \right) = \hat{\theta}_0, \quad (3.5b)$$

where $\hat{\theta}(t)$ stands for the result of the parameters $\theta(t)$ filtration, and $\gamma_1 > 0$ denotes the filter parameter.

Considering a particular case $\mathcal{K}(t) = \sin(t) + 2$ and T = 1, the relationship between the parameters $\mathcal{K}(t)$, $\theta(t)$ and $\hat{\theta}(t)$ is explained in Figs. 1a and 1b. For the same example, Fig. 1b demonstrates the approximation error $\delta_{\mathcal{K}0}(t)$ and its upper bound $\dot{\mathcal{K}}_{\max}T = 1$.

The conditions, under which the stated goal is achieved by application of the law (3.5a) + (3.5b), are presented in the following proposition.

Proposition 1. If the condition $i \leq i_{\max} < \infty$ is met, then there exists $T_{\min} > 0$ such that for all $0 < T < T_{\min}$ the control law (3.5) ensures that the stated goal (2.3) is achieved.

Proof of proposition is postponed to Appendix.

According to Proposition 1, in order to solve the stated problem (2.3), it is sufficient to use piecewise-constant approximations $\theta(t)$ of the time-varying parameters of the disturbance $\mathcal{K}^{\mathrm{T}}(t)\omega(t)$ to calculate the parameters of the control law (3.5a). Thus the adaptive control problem for a class

of systems with unknown time-varying parameters (2.1) is reduced to the one of identification of the unknown piecewise-constant parameters $\theta(t)$. To solve this problem, it is natural to be based jointly on approaches previously developed in [16, 19].

Remark 1. The condition $i \leq i_{\text{max}} < \infty$ is required for formal proof of proposition 1 and is not restrictive for practical scenarios.

4. MAIN RESULT

Following the method of exponentially stable adaptive control of systems with piecewise-constant parameters [19], for indirect implementation of (3.5), we first obtain a regression equation relating the parameters $\theta(t)$ to the signals calculated on the basis of the measurable vector $\Phi(t)$. The result of such a parameterisation can be formulated as a proposition.

Proposition 2. Using the state of the stable filter (l > 0) with resetting at some time instants t_i^+

$$\dot{\overline{\Phi}}(t) = -l\overline{\Phi}(t) + \Lambda^{\mathrm{T}}\left(t, t_{i}^{+}\right) \Phi\left(t\right), \quad \overline{\Phi}\left(t_{i}^{+}\right) = 0_{2(n+1)},
\Lambda\left(t, t_{i}^{+}\right) = \left[I_{n+1}\left(t - t_{i}^{+}\right)I_{n+1}\right] \in \mathbb{R}^{(n+1)\times 2(n+1)},$$
(4.1)

normalization procedure

$$\overline{z}_{n}(t) = n_{s}(t) e_{n}^{\mathrm{T}} \left[x(t) - l\overline{x}(t) - A_{0}\overline{x}(t) \right],$$

$$\overline{\varphi}_{n}^{\mathrm{T}}(t) = n_{s}(t) \overline{\varphi}(t) = n_{s}(t) \left[\overline{\Phi}^{\mathrm{T}}(t) \ e^{-l(t-t_{i}^{+})} \right],$$

$$n_{s}(t) = \frac{1}{1 + \overline{\varphi}^{\mathrm{T}}(t) \overline{\varphi}(t)}, \quad \overline{x}(t) = \begin{bmatrix} I_{n \times n} \ 0_{n \times (n+2)} \end{bmatrix} \overline{\Phi}(t),$$
(4.2)

extension ($\sigma > 0$)

$$\dot{z}(t) = e^{-\sigma\left(t - t_i^+\right)}\overline{\varphi}_n(t)\overline{z}_n^{\mathrm{T}}(t), \quad z\left(t_i^+\right) = 0_{2n+3},\tag{4.3a}$$

$$\dot{\varphi}(t) = e^{-\sigma(t-t_i^+)}\overline{\varphi}_n(t)\,\overline{\varphi}_n^{\mathrm{T}}(t)\,,\quad \varphi\left(t_i^+\right) = 0_{(2n+3)\times(2n+3)},\tag{4.3b}$$

mixing

$$Y(t) := \operatorname{adj} \left\{ \varphi(t) \right\} z(t), \quad \Delta(t) := \det \left\{ \varphi(t) \right\}, \tag{4.4}$$

elimination

$$z_{a}(t) = Y^{\mathrm{T}}(t) \mathfrak{L}_{a}, \quad z_{b}(t) = Y^{\mathrm{T}}(t) \mathfrak{L}_{b},$$
$$\mathfrak{L}_{a} = \begin{bmatrix} I_{n \times n} & 0_{n \times (n+3)} \end{bmatrix}^{\mathrm{T}} \in \mathbb{R}^{(2n+3) \times n}, \quad \mathfrak{L}_{b} = \begin{bmatrix} 0_{1 \times n} & 1 & 0_{1 \times (n+2)} \end{bmatrix}^{\mathrm{T}} \in \mathbb{R}^{(2n+3) \times 1},$$

$$(4.5)$$

substitution

$$\mathcal{V}(t) := \begin{bmatrix} \Delta(t) a_{ref}^{\mathrm{T}} - z_a(t) & \Delta(t) b_{ref} \end{bmatrix}^{\mathrm{T}}, \quad \mathcal{M}(t) := z_b(t), \quad (4.6)$$

and smoothing (k > 0)

$$\dot{\Upsilon}(t) = -k\left(\Upsilon(t) - \mathcal{Y}(t)\right), \quad \Upsilon\left(t_0^+\right) = 0_{n+1}, \tag{4.7a}$$

$$\dot{\Omega}(t) = -k\left(\Omega\left(t\right) - \mathcal{M}\left(t\right)\right), \quad \Omega\left(t_{0}^{+}\right) = 0, \tag{4.7b}$$

we have a perturbed regression equation

$$\Upsilon(t) = \Omega(t) \theta(t) + w(t), \qquad (4.8)$$

where the signals $\Upsilon(t)$, $\Omega(t)$ are calculated via $\Phi(t)$ and additionally:
a) if $\Phi \in \text{PE} \Rightarrow \overline{\varphi}_n \in \text{PE}$ with the period $T_s < T$, then there exists $T_{\min} > 0$ such that for all $0 < T < T_{\min}$ and $t \ge t_0^+ + T_s$ it holds that

$$0 < \Omega_{\rm LB} \leq \Omega(t) \leq \Omega_{\rm UB}.$$

b) if $i \leq i_{\max} < \infty$, then for all $t \geq t_0^+ + T_s$ it holds that

$$\|w(t)\| \leq w_{1\max} e^{-\gamma_1 \left(t - t_0^+ - T_s\right)} + w_{2\max}(T),$$
$$\lim_{T \to 0} w_{2\max}(T) = 0.$$

Proof of proposition and definition of w(t) are given in Appendix.

The parameterisation (4.1)–(4.8) uses the procedures proposed to solve the problem of adaptive control of systems with piecewise-constant parameters [19]. The difference is that the time-varying matrix $\Lambda(t, t_i^+)$ is used in (4.1) and the states of the filters (4.1) and (4.3) are reset at known, rather than algorithmically detectable, time instants.

Here we briefly explain the purpose of the procedures in use. Having the measurable signals $\Phi(t)$ at hand, the application of the filter (4.1) allows one to obtain a regression equation with measurable regressor and regressand with respect to parameters $\overline{\vartheta}(t) = \left[\Theta_i^T \quad \dot{\Theta}_i^T \quad e_n^T x\left(t_i^+\right)\right]^T$, where $\Theta\left(t_i^+\right) = \Theta_i$, $\dot{\Theta}\left(t_i^+\right) = \dot{\Theta}_i$ are the values of the system parameters $\Theta(t)$ and the rate of their change at the time instant t_i^+ . The normalisation (4.2) ensures that all signals used in further procedures belong to L_∞ space. The extension and mixing procedures (4.3), (4.4) allow one to transform the vector regressor $\overline{\varphi}_n(t) \in \mathbb{R}^{2n+3}$ into a scalar one $\Delta(t) \in \mathbb{R}$. Owing to $\Delta(t) \in \mathbb{R}$, the elimination (4.5) separates the regression equation under consideration into two ones with respect to the parameters of the piecewise-constant approximation of a(t) and b(t). By substitution (4.6) of (4.5) into the matching conditions (see assumption 2), we transform the equations with respect to approximation of the system parameters. Smoothing (4.7a), (4.7b) allows one to ensure sufficient smoothness of the signals $\Upsilon(t)$ and $\Omega(t)$.

Having at hand the regression equation (4.8) that regressor and regressand are based only on measurable signals $\Phi(t)$, we can indirectly implement the law (3.5) and guarantee the achievement of the goal (2.3).

Theorem 1. Let $\Phi \in PE \Rightarrow \overline{\varphi}_n \in PE$ with the period $T_s < T$, Assumptions 1–2 be met, then there exists $T_{\min} > 0$ such that for all $0 < T < T_{\min}$ the control law (3.5a) with the adaptive law

$$\dot{\hat{\theta}}(t) = -\gamma(t) \Omega(t) \left(\Omega(t) \hat{\theta}(t) - \Upsilon(t) \right)$$

$$= -\gamma(t) \Omega^{2}(t) \tilde{\theta}(t) + \gamma(t) \Omega(t) w(t), \quad \hat{\theta}\left(t_{0}^{+}\right) = \hat{\theta}_{0},$$

$$\gamma(t) = \begin{cases} 0, & \text{if } \Omega(t) < \rho \in (0, \Omega_{\text{LB}}], \\ \frac{\gamma_{1}}{\Omega^{2}(t)} & \text{otherwise}, \end{cases}$$
(4.9)

in case $i \leq i_{\max} < \infty$ for $\xi(t) = \begin{bmatrix} e_{ref}^{\mathrm{T}}(t) & vec^{\mathrm{T}}(\tilde{\theta}(t)) \end{bmatrix}^{\mathrm{T}}$, ensures that:

- 1) $\forall t \ge t_0^+ \quad \xi(t) \in L_\infty,$
- 2) $\lim_{t \to \infty} \|\xi(t)\| \leq \Delta_{\xi}(T) \text{ (exp)}, \quad \lim_{T \to 0} \Delta_{\xi}(T) = 0.$

Proof of theorem is presented in Appendix.



Fig. 2. Block diagram of proposed adaptive control system.

The block diagram of the obtained algorithm for adaptive control of systems with time-varying unknown parameters (2.1) is presented in Fig. 2.

Thus, the developed control system consists of a control law (3.5a), an adaptive law (4.9), a set of procedures (4.1)–(4.7) to process the measurable signals. In contrast to existing adaptive control methods [4–14], the proposed approach does not require any *a priori* information about the system parameters a(t) and b(t), does not use high-gain in control or adaptive laws, guarantees global exponential convergence of the error $\xi(t)$ to the bounded neighbourhood of the equilibrium, which can be adjusted by the parameter T.

Remark 2. The feature of the proposed solution is the relationship between the steady-state error $\Delta_{\xi}(T)$, the length of the Taylor series expansion interval T and the period of the regressor persistent excitation T_s . The problem is that the parameter T cannot be made smaller than the value of the regressor excitation period T_s . However, for a fixed period T_s and a minimum possible $T < T_{\min}$ such that $T - T_s > 0$, the error $\xi(t)$ may be bounded in an unacceptably large neighbourhood of the equilibrium point $\Delta_{\xi}(T)$. Therefore, in order to reduce the steady-state error, it is necessary, first of all, to ensure a persistent excitation of the regressor with a sufficiently small period T_s , which in practice can be achieved by addition of a high-frequency or random test signal to the reference r(t).

5. NUMERICAL EXPERIMENTS

In Matlab/Simulink numerical experiments have been conducted for the proposed adaptive system using the explicit Euler solver with a constant step time of $\tau_s = 10^{-3}$ s.

The system (2.1) was considered with n = 2. The initial conditions, the parameters of the system and reference model (2.2) were chosen as

$$x_{0} = \begin{bmatrix} -1 & 1 \end{bmatrix}^{\mathrm{T}}, \quad b(t) = 3 + \cos(0.4t)\sin(0.1t), \quad a_{ref}^{\mathrm{T}}(t) = \begin{bmatrix} -8 & -4 \end{bmatrix}, \\ a^{\mathrm{T}}(t) = \begin{bmatrix} 2 + \sin(0.1t) & 1 + 5\left(1 - e^{\frac{-1}{25}t}\right) \end{bmatrix}, \quad b_{ref} = 8.$$
(5.1)

First, we verified the preliminary conclusions made in Proposition 1. We picked $\gamma_1 = 50$ as the filter constant (3.5b), and defined the reference as r(t) = 10. Figure 3 presents the comparison of the error $e_{1ref}(t)$ for different T.

The obtained results validated the conclusions made in Proposition 1. Indeed, a decrease of T resulted in a decrease of the steady-state value of the tracking error $e_{ref}(t)$ when the control law (3.5a) with (3.5b) was applied. Having checked proposition 1, we proceeded to verify the main result.



Fig. 3. Behavior of $|e_{1ref}(t)|$ for different T.



Fig. 4. Behavior of regressors $\mathcal{M}(t)$ and $\Omega(t)$.

The parameters of the filters (4.1), (4.3), (4.7) and the adaptive law (4.9) were chosen as

$$l = 10, \quad \sigma = \frac{0.05}{T}, \quad k = 50, \quad \rho = 10^{-72}, \quad \gamma_1 = 100, \quad T = 0.25,$$

the reference was picked as $r(t) = 1 + r_d(t)$ for $r_d(t) \sim \mathcal{N}(0, 10^{-2})$. A random signal $r_d(t)$ was added to a unity reference signal to ensure that $\overline{\varphi}_n \in \text{PE}$ for the closed-loop system (3.1).

Figure 4 depicts the behavior of the regressors $\mathcal{M}(t)$ and $\Omega(t)$ on the logarithmic scale.

It follows from the obtained results that despite the fact that the filters (4.1) and (4.3) were reset every T seconds, the regressor $\Omega(t)$ (unlike $\mathcal{M}(t)$) was globally bounded away from zero starting from some time instant, which confirms the theoretical conclusions made in statement (a) of Proposition 2. Figure 4 demonstrates the importance of the smoothing procedure (4.7), which, as can be seen, allows one to (i) average the values of the regressor $\mathcal{M}(t)$ over the period T, and (ii) avoid discontinuities caused by the reinitialisation of the filters (4.1) and (4.3).

Figure 5 shows the behavior of (a) the state x(t) when the control law (3.5a) with (3.5b) and with (4.9) is used, (b) the estimates of $\hat{\theta}_i(t)$ and the true parameters $\theta_i(t) + 1$ shifted by one for clarity of illustration, (c) the control signal (3.5a) with (4.9).

Figure 6 compares the values of the integral control quality index of tracking $e_{ref}(t)$ and parametric $\tilde{\theta}(t)$ errors for different values of T.

The simulation results illustrate the conclusions of Propositions 1, 2 and theorem. The goal (2.3) is achieved, and the steady-state values of the errors $e_{ref}(t)$ and $\tilde{\theta}(t)$ are directly proportional to the parameter T.



Fig. 5. Behavior of (a)–(b) state x(t) when control law (3.5a) used with (3.5b) and with (4.9), (c) estimates $\hat{\theta}_i(t)$ and ideal parameters $\theta_i(t) + 1$ shifted by one for clarity of illustration, (d) control signal (3.5a) with (4.9).



Fig. 6. Comparison of integral control quality indexes.

6. CONCLUSION

The problem of tracking of a linear time-invariant reference model by a linear time-varying system is solved. It is proposed to approximate the unknown time-varying parameters of the ideal control law by piecewise-constant parameters. Parametric identification methods proposed in [16, 19] are combined to identify these piecewise-constant parameters. The resulting adaptive control system requires persistent excitation of the regressor with a sufficiently small period to achieve the control goal, but it does not require *a priori* information about the unknown parameters of the system.

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APPENDIX

Proof of Proposition 1. The proof of the proposition is divided into two steps. At the first one we analyse the properties of the parametric error $\tilde{\theta}(t)$, at the second one — the properties of the tracking error $e_{ref}(t)$.

Step 1. Owing to proposition 1 from [19], if $i \leq i_{\text{max}} < \infty$, then for the differential equation

$$\dot{\tilde{\theta}}(t) = -\gamma_1 \tilde{\theta}(t) - \dot{\theta}(t), \quad \tilde{\theta}\left(t_0^+\right) = \hat{\theta}_0 - \theta\left(t_0^+\right)$$

the following upper bound holds

$$\left\|\tilde{\theta}\left(t\right)\right\| \leqslant \beta_{\max} e^{-\gamma_1 \left(t - t_0^+\right)}, \quad \beta_{\max} > 0, \tag{A.1}$$

where $\dot{\theta}(t) = \sum_{q=1}^{i} \Delta_q^{\theta} \delta\left(t - t_q^+\right)$, and $\delta: [t_0^+; \infty) \to \{0, \infty\}$ is the Dirac function.

Step 2. The following quadratic form is introduced:

$$V_{e_{ref}} = e_{ref}^{\mathrm{T}} P e_{ref} + \frac{a_0^2}{\gamma_1} e^{-2\gamma_1 \left(t - t_0^+\right)}, \quad H = \text{blockdiag} \left\{ P, \ \frac{a_0^2}{\gamma_1} \right\},$$

$$\underbrace{\lambda_{\min}\left(H\right)}_{\lambda_{\mathrm{m}}} \|\overline{e}_{ref}\|^2 \leqslant V\left(\|\overline{e}_{ref}\|\right) \leqslant \underbrace{\lambda_{\max}\left(H\right)}_{\lambda_M} \|\overline{e}_{ref}\|^2, \tag{A.2}$$

where $\overline{e}_{ref}(t) = \begin{bmatrix} e_{ref}^{\mathrm{T}}(t) & e^{-\gamma_1(t-t_0^+)} \end{bmatrix}^{\mathrm{T}}, P = P^{\mathrm{T}} > 0$ is the solution of the below-given Lyapunov equation in case $\lambda_{\min}(Q) > 2$:

$$A_{ref}^{\rm T}P + PA_{ref} = -Q, \quad Q = Q^{\rm T} > 0.$$

The derivative of the quadratic form (A.2) is written as:

$$\begin{split} \dot{V}_{e_{ref}} &= e_{ref}^{\mathrm{T}} \left(A_{ref}^{\mathrm{T}} P + P A_{ref} \right) e_{ref} - 2a_{0}^{2} e^{-2\gamma_{1} \left(t - t_{0}^{+} \right)} + 2e_{ref}^{\mathrm{T}} P e_{n} b \tilde{\theta}^{\mathrm{T}} \omega + 2e_{ref}^{\mathrm{T}} P e_{n} b \delta_{\theta_{0}}^{\mathrm{T}} \omega \\ &= -e_{ref}^{\mathrm{T}} Q e_{ref} - 2a_{0}^{2} e^{-2\gamma_{1} \left(t - t_{0}^{+} \right)} + 2e_{ref}^{\mathrm{T}} P e_{n} b \tilde{\theta}^{\mathrm{T}} \left(\omega_{e_{ref}} + \omega_{r} \right) + 2e_{ref}^{\mathrm{T}} P e_{n} b \delta_{\theta_{0}}^{\mathrm{T}} \left(\omega_{e_{ref}} + \omega_{r} \right) \\ &\leq -\lambda_{\min} \left(Q \right) \| e_{ref} \|^{2} - 2a_{0}^{2} e^{-2\gamma_{1} \left(t - t_{0}^{+} \right)} \\ &+ 2\lambda_{\max} \left(P \right) b_{\max} \| e_{ref} \|^{2} \left\| \tilde{\theta} \right\| + 2\lambda_{\max} \left(P \right) \overline{\omega}_{r} b_{\max} \| e_{ref} \| \left\| \tilde{\theta} \right\| \\ &+ 2\lambda_{\max} \left(P \right) b_{\max} \dot{\mathcal{K}}_{\max} T \| e_{ref} \|^{2} + 2\lambda_{\max} \left(P \right) b_{\max} \overline{\omega}_{r} \dot{\mathcal{K}}_{\max} T \| e_{ref} \| \,, \end{split}$$
(A.3)

where

$$\|\omega\left(t\right)\| \leqslant \underbrace{\left\| \begin{bmatrix} e_{ref}\left(t\right) & 0 \end{bmatrix} \right\|}_{\left\|\omega_{e_{ref}}\left(t\right)\right\| = \left\|e_{ref}\left(t\right)\right\|} + \underbrace{\left\| \begin{bmatrix} x_{ref}\left(t\right) & r\left(t\right) \end{bmatrix} \right\|}_{\left\|\omega_{r}\left(t\right)\right\| \leqslant \overline{\omega}_{r}} \leqslant \left\|e_{ref}\left(t\right)\right\| + \overline{\omega}_{r}$$

Having applied Young's inequality twice:

$$2\lambda_{\max}(P)\overline{\omega}_{r}b_{\max}\|e_{ref}\|\left\|\tilde{\theta}\right\| \leq \|e_{ref}\|^{2} + \lambda_{\max}^{2}(P)\overline{\omega}_{r}^{2}b_{\max}^{2}\left\|\tilde{\theta}\right\|^{2},$$

$$2\lambda_{\max}(P)b_{\max}\overline{\omega}_{r}\dot{\mathcal{K}}_{\max}T\|e_{ref}\| \leq \lambda_{\max}^{2}(P)b_{\max}^{2}\overline{\omega}_{r}^{2}\dot{\mathcal{K}}_{\max}^{2}T^{2} + \|e_{ref}\|^{2},$$
(A.4)

~

equation (A.3) is rewritten as:

$$\dot{V}_{e_{ref}} \leqslant \left[-\lambda_{\min}\left(Q\right) + 2\lambda_{\max}\left(P\right)b_{\max}\left(\left\|\tilde{\theta}\right\| + \dot{\mathcal{K}}_{\max}T\right) + 2 \right] \|e_{ref}\|^2 -2a_0^2 e^{-2\gamma_1\left(t-t_0^+\right)} + \lambda_{\max}^2\left(P\right)\overline{\omega}_r^2 b_{\max}^2 \left\|\tilde{\theta}\right\|^2 + \lambda_{\max}^2\left(P\right) b_{\max}^2 \overline{\omega}_r^2 \dot{\mathcal{K}}_{\max}^2 T^2.$$
(A.5)

As the parametric error $\tilde{\theta}(t)$ converges to zero exponentially (A.2), then, if $\lambda_{\min}(Q) > 2$, then there definitely exists a time instant $t_{e_{ref}} \ge t_0^+$ and constants $T_{\min} > 0$, $a_0 > \lambda_{\max}(P) \overline{\omega}_r b_{\max} \beta_{\max}$ such that for all $t \ge t_{e_{ref}}$ and $0 < T < T_{\min}$ it holds that

$$-\lambda_{\min}(Q) + 2\lambda_{\max}(P) b_{\max}\left(\beta_{\max}e^{-\gamma_1\left(t_{e_{ref}} - t_0^+\right)} + \dot{\mathcal{K}}_{\max}T\right) + 2 = -c_1 < 0,$$

$$\lambda_{\max}^2(P) \overline{\omega}_r^2 b_{\max}^2 \beta_{\max}^2 - 2a_0^2 = -c_2 < 0.$$
(A.6)

Then the upper bound of the derivative (A.5) for all $t \ge t_{e_{ref}}$ is written as

$$\dot{V}_{e_{ref}} \leqslant -\eta_{\overline{e}_{ref}} V_{e_{ref}} + \lambda_{\max}^2 \left(P\right) b_{\max}^2 \overline{\omega}_r^2 \dot{\mathcal{K}}_{\max}^2 T^2, \tag{A.7}$$

where $\eta_{\overline{e}_{ref}} = \min\left\{\frac{c_1}{\lambda_{\max}(P)}, \frac{c_2\gamma_1}{a_0^2}\right\}$.

The solution of the differential inequality (A.7) for all $t \ge t_{e_{ref}}$ is obtained as

$$V_{e_{ref}}(t) \leqslant e^{-\eta_{\overline{e}_{ref}}} \left(t - t_{e_{ref}}\right) V_{e_{ref}}\left(t_{e_{ref}}\right) + \frac{\lambda_{\max}^2 \left(P\right) b_{\max}^2 \overline{\omega}_r^2 \dot{\mathcal{K}}_{\max}^2 T^2}{\eta_{\overline{e}_{ref}}}.$$
 (A.8)

Tending time to infinity for (A.8) and considering expression for $V_{e_{ref}}$, it is concluded that (2.3) holds, which completes the proof.

Proof of Proposition 2. Owing to assumption 2 and following (3.2)–(3.3), we apply the Taylor formula (1.3) to the parameters $\Theta(t)$ to obtain:

$$\Theta(t) = \Theta\left(t_i^+\right) + \overleftarrow{\Theta}\left(t_i^+\right)\left(t - t_i^+\right) + \underbrace{\int_{t_i}^t (t - \zeta)\ddot{\Theta}\left(\zeta\right)d\zeta}_{\delta_1(t)}, \tag{A.9}$$

where $\Theta(t_i^+) = \Theta_i$, $\dot{\Theta}(t_i^+) = \dot{\Theta}_i$ are the values of the system parameters $\Theta(t)$ and the rate of their change at the time instant t_i^+ , $\|\delta_1(t)\| \leq 0.5 \ddot{\Theta}_{\max} T^2$ denotes the bounded reminder of the first order (p = 1), $\|\delta_0(t)\| \leq \dot{\Theta}_{\max} T$ is the bounded reminder of the zeroth order (p = 0).

Equation (A.9) is rewritten in the matrix form

$$\Theta(t) = \Lambda\left(t, t_i^+\right)\vartheta(t) + \delta_1(t), \qquad (A.10)$$

where $\vartheta(t) = \begin{bmatrix} \Theta_i^{\mathrm{T}} & \dot{\Theta}_i^{\mathrm{T}} \end{bmatrix}^{\mathrm{T}} \in \mathbb{R}^{2(n+1)}.$

The substitution of (A.10) into (2.1) yields

$$\dot{x}(t) = A_0 x + e_n \left(\Phi^{\mathrm{T}}(t) \Lambda\left(t, t_i^+\right) \vartheta\left(t\right) + \Phi^{\mathrm{T}}(t) \delta_1\left(t\right) \right).$$
(A.11)

The expression $x(t) - l\overline{x}(t)$ is differentiated to obtain

$$\dot{x}(t) - l\dot{\overline{x}}(t) = -l\left(x\left(t\right) - l\overline{x}\left(t\right)\right) + A_0 x + e_n\left(\Phi^{\mathrm{T}}(t)\Lambda\left(t,t_i^{+}\right)\vartheta\left(t\right) + \Phi^{\mathrm{T}}(t)\delta_1\left(t\right)\right).$$
(A.12)

The solution of (A.12) is written as

$$x(t) - l\overline{x}(t) = e^{-l(t-t_i^+)}x(t_i) + A_0\overline{x}(t) + \int_{t_i^+}^t e^{-l(t-\tau)}e_n\Phi^{\mathrm{T}}(\tau)\Lambda\left(\tau, t_i^+\right)\vartheta\left(\tau\right)d\tau$$

$$+ \int_{t_i^+}^t e^{-l(t-\tau)}e_n\Phi^{\mathrm{T}}(\tau)\delta_1(\tau)d\tau = A_0\overline{x}(t) + e_n\overline{\varphi}(t)\overline{\vartheta}(t) + e_n\int_{t_i^+}^t e^{-l(t-\tau)}\Phi^{\mathrm{T}}(\tau)\delta_1(\tau)d\tau, \qquad (A.13)$$

$$\underbrace{\sum_{t_i^+}^{t_i^+}e^{-l(t-\tau)}e_n\Phi^{\mathrm{T}}(\tau)\delta_1(\tau)d\tau}_{\varepsilon_0(t)} = A_0\overline{x}(t) + e_n\overline{\varphi}(t)\overline{\vartheta}(t) + e_n\int_{t_i^+}^t e^{-l(t-\tau)}\Phi^{\mathrm{T}}(\tau)\delta_1(\tau)d\tau,$$

where $\overline{\vartheta}(t) = \begin{bmatrix} \vartheta^{\mathrm{T}}(t) & e_n^{\mathrm{T}}x\left(t_i^+\right) \end{bmatrix}^{\mathrm{T}} \in \mathbb{R}^{2n+3}$, and the third equality is not violated since the reset of the filter states (4.1) and the change of parameters occur synchronously at a known time instant t_i^+ , i.e. $\overline{\vartheta}(t) = \text{const for all } t \in [t_i^+, t_i^+ + T]$.

Equation (A.13) is substituted into (4.2) to obtain

$$\overline{z}_{n}(t) = n_{s}(t) e_{n}^{\mathrm{T}}[x(t) - l\overline{x}(t) - A_{0}\overline{x}(t)] = \overline{\varphi}_{n}^{\mathrm{T}}(t) \overline{\vartheta}(t) + \overline{\varepsilon}_{0}(t), \qquad (A.14)$$

where $\overline{z}_n(t) \in \mathbb{R}$, $\overline{\varphi}_n(t) \in \mathbb{R}^{2n+3}$ and the perturbation $\overline{\varepsilon}_0(t) \in \mathbb{R}$ is bounded as follows (see definitions of $\Phi(t)$ and $\overline{\varphi}_n(t)$):

$$\left\|\overline{\varepsilon}_{0}\left(t\right)\right\| = \left\|n_{s}\left(t\right)\int_{t_{i}^{+}}^{t}e^{-l\left(t-\tau\right)}\Phi^{\mathrm{T}}\left(\tau\right)\delta_{1}\left(\tau\right)d\tau\right\| \leqslant \left\|\overline{\varphi}_{n}^{\mathrm{T}}\left(t\right)\right\|0.5\ddot{\Theta}_{\mathrm{max}}T^{2}.$$
(A.15)

Owing to the multiplication of the regression equation (A.14) by $n_s(t)$, the regressor $\overline{\varphi}_n^{\mathrm{T}}(t)$, the regressand $\overline{z}_n(t)$ and the perturbation $\overline{\varepsilon}_0(t)$ are bounded. In addition, according to the upper bound (A.15), the perturbation $\overline{\varepsilon}_0(t)$ can be reduced by decreasing the parameter T. Therefore, further on we will use the definition $\overline{\varepsilon}_0(t) := \overline{\varepsilon}_0(t, T)$ and imply that any perturbation obtained by transformation of $\overline{\varepsilon}_0(t, T)$ can also be reduced by a reduction of T.

Having applied (4.3) and multiplicated z(t) by adj $\{\varphi(t)\}$, we have (commutativity of the filter (4.3a) is not violated as its reinitialization and parameters change happen synchronously at a known time instant t_i^+ , *i.e.* $\overline{\vartheta}(t) = \text{const for all } t \in [t_i^+, t_i^+ + T)$)

$$Y(t) := \operatorname{adj} \{\varphi(t)\} z(t) = \Delta(t) \overline{\vartheta}(t) + \overline{\varepsilon}_{1}(t, T),$$

$$\operatorname{adj} \{\varphi(t)\} \varphi(t) = \operatorname{det} \{\varphi(t)\} I_{2(n+1)+1} = \Delta(t) I_{2(n+1)+1},$$

$$\overline{\varepsilon}_{1}(t, T) = \operatorname{adj} \{\varphi(t)\} \int_{t_{i}^{+}}^{t} e^{-\sigma(\tau - t_{i}^{+})} \overline{\varphi}_{n}(\tau) \overline{\varepsilon}_{0}(\tau, T) d\tau,$$

(A.16)

where $Y(t) \in \mathbb{R}^{2n+3}$, $\Delta(t) \in \mathbb{R}$, $\overline{\varepsilon}_1(t, T) \in \mathbb{R}^{2n+3}$.

Owing to $\Delta(t) \in \mathbb{R}$, the elimination (4.5) allows one to obtain the following from (A.16)

$$z_{a}(t) = Y^{\mathrm{T}}(t) \mathfrak{L}_{a} = \Delta(t) \vartheta_{a}^{\mathrm{T}}(t) + \overline{\varepsilon}_{1}^{\mathrm{T}}(t, T) \mathfrak{L}_{a},$$

$$z_{b}(t) = Y^{\mathrm{T}}(t) \mathfrak{L}_{b} = \Delta(t) \vartheta_{b}(t) + \overline{\varepsilon}_{1}^{\mathrm{T}}(t, T) \mathfrak{L}_{b},$$
(A.17)

where $z_a(t) \in \mathbb{R}^{1 \times n}$, $z_b(t) \in \mathbb{R}$, and $\vartheta_a(t)$, $\vartheta_b(t)$ are the first order approximations of the parameters a(t) and b(t), respectively (components of the vector Θ_i).

In case Assumption 2 is met, following the definition of the signal $\mathcal{K}(t)$, the first order approximations $\theta_x(t)$ and $\theta_r(t)$ of the parameters $k_x(t)$ and $k_r(t)$, respectively, satisfy the equations

$$a_{ref}^{\mathrm{T}} - \vartheta_{a}^{\mathrm{T}}(t) = \vartheta_{b}(t) \,\theta_{x}(t) \,, \ b_{ref} = \vartheta_{b}(t) \,\theta_{r}(t) \,. \tag{A.18}$$

where $\theta(t) = \begin{bmatrix} \theta_x(t) & \theta_r(t) \end{bmatrix}^{\mathrm{T}}$.

Each equation from (A.18) is multiplied by $\Delta(t)$. Equations (A.17) are substituted into the obtained result to have equation (4.6):

$$\mathcal{Y}(t) = \mathcal{M}(t) \theta(t) + d(t, T),$$

$$\mathcal{Y}(t) := \begin{bmatrix} \Delta(t) a_{ref}^{\mathrm{T}} - z_a(t) & \Delta(t) b_{ref} \end{bmatrix}^{\mathrm{T}},$$

$$\mathcal{M}(t) := z_b(t),$$

$$d(t, T) := -\begin{bmatrix} \overline{\varepsilon}_1^{\mathrm{T}}(t, T) \mathfrak{L}_a + \overline{\varepsilon}_1^{\mathrm{T}}(t, T) \mathfrak{L}_b \theta_r(t) & \overline{\varepsilon}_1^{\mathrm{T}}(t, T) \mathfrak{L}_b \theta_r(t) \end{bmatrix}^{\mathrm{T}},$$

(A.19)

where $\mathcal{Y}(t) \in \mathbb{R}^{n+1}$, $\mathcal{M}(t) \in \mathbb{R}$, $d(t, T) \in \mathbb{R}^{n+1}$.

Owing to (A.19), the solution of (4.7a) is written as

$$\Upsilon(t) = \int_{t_0^+}^t e^{\int_t^\tau k d\tau} \mathcal{M}(\tau) \theta(\tau) d\tau + \int_{t_0^+}^t e^{\int_t^\tau k d\tau} d(\tau, T) d\tau \pm \Omega(t) \theta(t) = \Omega(t) \theta(t) + w(t), \quad (A.20)$$

where

$$w(t) = \Upsilon(t) - \Omega(t) \theta(t).$$

Equation (A.20) completes the proof of the fact that equation (4.8) can be obtained via procedure (4.1)-(4.7).

In order to prove statement (a), the regressor $\Omega(t)$ is represented as:

$$\Omega(t) = \Omega_1(t) + \Omega_2(t),$$

$$\dot{\Omega}_1(t) = -k\left(\Omega_1(t) - \Delta(t)\vartheta_b(t)\right), \quad \Omega_1\left(t_0^+\right) = 0,$$

$$\dot{\Omega}_2(t) = -k\left(\Omega_2(t) - \overline{\varepsilon}_1^{\mathrm{T}}(t, T)\mathfrak{L}_b\right), \quad \Omega_2\left(t_0^+\right) = 0.$$
(A.21)

As k > 0 and the perturbation $\overline{\varepsilon}_1(t, T)$ is bounded, then $\Omega_2(t)$ is bounded, moreover, for all $t \ge t_0^+$ the following holds

$$\left|\Omega_{2}\left(t\right)\right| \leqslant \Omega_{2\max}\left(T\right),\tag{A.22}$$

and there exists a limit $\lim_{T\to 0} \Omega_{2\max}(T) = 0$ for the upper bound as, following (A.15)–(A.19), the value of $\overline{\varepsilon}_1(t, T)$ can be arbitrarily reduced by reduction of T.

The next aim is to analyze $\Omega_1(t)$. The solution of the first differential equation from (A.21) is written for all $t \in [t_i^+ + T_s, t_{i+1}^+)$ as

$$\Omega_1(t) = \phi\left(t, t_i^+ + T_s\right) \Omega_1\left(t_i^+ + T_s\right) + \int_{t_i^+ + T_s}^t \phi\left(t, \tau\right) \Delta\left(\tau\right) \vartheta_b\left(\tau\right) d\tau, \qquad (A.23)$$

where $\phi(t,\tau) = e^{-\int_{\tau}^{t} k d\tau}$.

The upper bound is required for the signal $\Omega_1(t)$ over the time range under consideration. To this end, we need bounds for $\Delta(t)$, and, in its turn, the ones for $\varphi(t)$.

As, according to the premises of the proposition, $\overline{\varphi}_n \in \text{PE}$ for $T_s < T$, then $\overline{\varphi}_n \in \text{FE}$ over $\begin{bmatrix} t_i^+, t_i^+ + T_s \end{bmatrix}$ (this fact can be validated by substitution of $t = t_i^+$ into (1.2)). Then for all $t \in \begin{bmatrix} t_i^+ + T_s, t_{i+1}^+ \end{bmatrix}$ the following lower bound holds for the regressor $\varphi(t)$

$$\varphi(t) = \int_{t_i^+}^t e^{-\sigma\left(\tau - t_i^+\right)} \overline{\varphi}_n(\tau) \,\overline{\varphi}_n^{\mathrm{T}}(\tau) \,d\tau$$

$$\geqslant \int_{t_i^+}^{t_i^+ + T_s} e^{-\sigma\left(\tau - t_i^+\right)} \overline{\varphi}_n(\tau) \,\overline{\varphi}_n^{\mathrm{T}}(\tau) \,d\tau \qquad (A.24)$$

$$e^{-\sigma\left(t_{i+1}^+ - t_i^+\right)} \int_{t_i^+}^{t_i^+ + T_s} \overline{\varphi}_n(\tau) \,\overline{\varphi}_n^{\mathrm{T}}(\tau) \,d\tau \geqslant \alpha e^{-\sigma\left(t_{i+1}^+ - t_i^+\right)} I_{n+1}.$$

On the other hand, as $\|\overline{\varphi}_n(t)\|^2 \leqslant \overline{\varphi}_n^{\max}$, then there exists an upper bound

 \geq

$$\varphi(t) \leqslant \overline{\varphi}_n^{\max} \int_{t_i^+}^t e^{-\sigma\left(\tau - t_i^+\right)} d\tau \leqslant \overline{\varphi}_n^{\max} \frac{1 - e^{-\sigma\left(t - t_i^+\right)}}{\sigma} \leqslant \sigma^{-1} \overline{\varphi}_n^{\max}, \tag{A.25}$$

and, therefore, for all $t \in \left[t_i^+ + T_s, t_{i+1}^+\right)$ it holds that $\Delta_{UB} \ge \Delta(t) \ge \Delta_{LB} > 0$.

Taking into consideration that, following Assumptions 1 and 2, $b_{\max} \ge |b(t)| \ge b_{\min} > 0$, and $\vartheta_b(t)$ is the approximation of first order of b(t), then the following holds for the multiplication $\Delta(t) \vartheta_b(t)$

$$\forall t \in \left[t_{i}^{+} + T_{s}, t_{i+1}^{+}\right) \quad \Delta_{UB} b_{\max} \ge \left|\Delta\left(t\right)\vartheta_{b}\left(t\right)\right| \ge \Delta_{LB} b_{\min} > 0.$$
(A.26)

Having applied (A.21) and (A.26) and considered that $0 \leq \phi(t, \tau) \leq 1$, the following estimates hold for $\Omega_1(t)$

$$\forall t \in \begin{bmatrix} t_0^+, t_0^+ + T_s \end{bmatrix} \quad \Omega_1(t) \equiv 0,$$

$$\forall i \ge 1 \quad \forall t \in \begin{bmatrix} t_i^+ + T_s, t_{i+1}^+ \end{bmatrix} \quad \Omega_1\left(t_i^+ + T_s\right) + \left(t_{i+1}^+ - t_i^+ - T_s\right) \Delta_{UB} b_{\max} \ge \Omega_1(t)$$

$$\ge \phi\left(t_{i+1}^+, t_i^+ + T_s\right) \left(\Omega_1\left(t_i^+ + T_s\right) + \left(t_{i+1}^+ - t_i^+ - T_s\right) \Delta_{LB} b_{\min}\right) > 0,$$

$$(A.27)$$

from which we have

$$\forall t \ge t_0 + T_s \quad \Omega_{1\max} \ge \Omega_1(t) \ge \Omega_{1\min} > 0,$$

$$\Omega_{1\max} = \min_{\forall i \ge 1} \left\{ \phi \left(t_{i+1}^+, t_i^+ + T_s \right) \left(\Omega_1 \left(t_i^+ + T_s \right) + \left(t_{i+1}^+ - t_i^+ - T_s \right) \Delta_{LB} b_{\min} \right) \right\},$$

$$\Omega_{1\min} = \max_{\forall i \ge 1} \left\{ \Omega_1 \left(t_i^+ + T_s \right) + \left(t_{i+1}^+ - t_i^+ - T_s \right) \Delta_{UB} b_{\max} \right\}.$$

$$(A.28)$$

Then, using (A.28) and (A.23), the bounds for the regressor $\Omega(t)$ are written

$$\forall t \ge t_0 + T_s \ \Omega_{1\max} + \Omega_{2\max} \left(T \right) \ge \left| \Omega \left(t \right) \right| \ge \Omega_{1\min} - \Omega_{2\max} \left(T \right), \tag{A.29}$$

and, therefore, considering $\lim_{T\to 0} \Omega_{2\max}(T) = 0$, there exists $T_{\min} > 0$ such that for all $0 < T < T_{\min}$ and $t \ge t_0 + T_s$ the following inequality holds

$$\Omega_{\rm UB} \ge \Omega\left(t\right) \ge \Omega_{\rm LB} > 0,\tag{A.30}$$

which was to be proved in statement (a).

In order to prove the statement (b), the disturbance w(t) is differentiated with (A.20) and (4.7) at hand

$$\dot{w}(t) = \dot{\Upsilon}(t) - \dot{\Omega}(t)\theta(t) - \Omega(t)\dot{\theta}(t)$$

$$= -k\left(\Upsilon(t) - \mathcal{Y}(t)\right) + k\left(\Omega(t) - \mathcal{M}(t)\right)\theta(t) - \Omega(t)\dot{\theta}(t)$$

$$= -k\left(\Upsilon(t) - \mathcal{M}(t)\theta(t) - d(t,T)\right) + k\left(\Omega(t) - \mathcal{M}(t)\right)\theta(t) - \Omega(t)\dot{\theta}(t) \qquad (A.31)$$

$$= -k\left(\Upsilon(t) - \Omega(t)\theta(t)\right) - \Omega(t)\dot{\theta}(t) + kd(t,T)$$

$$= -kw\left(t\right) - \Omega(t)\dot{\theta}(t) + kd(t,T), \quad w\left(t_{0}^{+}\right) = 0_{n+1}.$$

The solution of (A.31) is represented as:

$$w(t) = w_1(t) + w_2(t),$$

$$\dot{w}_1(t) = -kw_1(t) - \Omega(t)\dot{\theta}(t), \quad w_1(t_0^+) = 0_{n+1},$$

$$\dot{w}_2(t) = -kw_2(t) + kd(t, T), \quad w_2(t_0^+) = 0_{n+1}.$$

(A.32)

As for the first differential equation from (A.32), in Proposition 2 from [19] it is proved (up to notation) that the following inequality holds

$$||w_1(t)|| \leq w_{1\max}\phi\left(t, t_0^+ + T_s\right),$$
 (A.33)

when $i \leq i_{\max} < \infty$.

As k > 0 and the disturbance d(t, T) is bounded, then $w_2(t)$ is also bounded, and consequently, the following inequality holds

$$\|w_2(t)\| \leqslant w_{2\max}(T), \qquad (A.34)$$

where the limit $\lim_{T\to 0} w_{2\max}(T) = 0$ holds, as the input of the second differential equation from (A.32) depends only from the value of d(t, T), which, in its turn, according to (A.15)–(A.19), can be reduced arbitrarily by reduction of T. The combination of the inequalities (A.33) and (A.34) in accordance with (A.32) completes the proof of proposition.

Proof of Theorem 1. Proof of theorem is similar to the above-given proof of Proposition 1. Step 1. For all $t \ge t_0^+ + T_s$ the solution of the differential equation (4.9) is written as

$$\tilde{\theta}(t) = \phi\left(t, t_0^+ + T_s\right) \tilde{\theta}\left(t_0^+ + T_s\right) + \int_{t_0^+ + T_s}^t \phi\left(t, \tau\right) \frac{\gamma_1 w\left(\tau\right)}{\Omega\left(\tau\right)} d\tau$$

$$- \int_{t_0^+ + T_s}^t \phi\left(t, \tau\right) \sum_{q=1}^i \Delta_q^\theta \delta\left(\tau - t_q^+\right) d\tau,$$
(A.35)

where $\phi(t,\tau) = e^{-\int_{\tau}^{t} \gamma_1 d\tau}$.

Then, following the proof of Theorem 1 from [19], if $i \leq i_{\text{max}} < \infty$, then the boundedness of the parametric error (A.35) can be shown:

$$\left\| \tilde{\theta} \left(t \right) \right\| \leqslant \beta_{\max} e^{-\frac{\gamma_{1}}{2} \left(t - t_{0}^{+} - T_{0} \right)} + \frac{\gamma_{1} w_{1\max}}{\Omega_{LB}} \int_{t_{0}^{+} + T_{s}}^{t} \phi \left(t, \tau \right) \phi \left(\tau, t_{0}^{+} + T_{s} \right) d\tau + \frac{\gamma_{1} w_{2\max} \left(T \right)}{\Omega_{LB}} \int_{t_{0}^{+} + T_{s}}^{t} \phi \left(t, \tau \right) d\tau \leqslant \left(\beta_{\max} + \frac{2w_{1\max}}{\Omega_{LB}} \right) e^{-\frac{\gamma_{1}}{2} \left(t - t_{0}^{+} - T_{0} \right)} + \frac{\gamma_{1} w_{2\max} \left(T \right)}{\Omega_{LB}}.$$
(A.36)

Step 2. The following quadratic form is introduced for all $t \ge t_0^+ + T_s$:

$$V_{e_{ref}} = e_{ref}^{\mathrm{T}} P e_{ref} + \frac{4a_0^2}{\gamma_1} e^{-\frac{\gamma_1}{2} \left(t - t_0^+ - T_s\right)}, \quad H = \mathrm{blockdiag} \left\{ P, \frac{4a_0^2}{\gamma_1} \right\},$$

$$\underbrace{\lambda_{\min}\left(H\right)}_{\lambda_{\mathrm{m}}} \|\overline{e}_{ref}\|^2 \leqslant V\left(\|\overline{e}_{ref}\|\right) \leqslant \underbrace{\lambda_{\max}\left(H\right)}_{\lambda_{M}} \|\overline{e}_{ref}\|^2, \quad (A.37)$$

$$\overline{e}_{ref}\left(t\right) = \left[e_{ref}^{\mathrm{T}}\left(t\right) \quad e^{-\frac{\gamma_1}{4} \left(t - t_0^+ - T_s\right)} \right]^{\mathrm{T}}.$$

Similar to proof of Proposition 1, the derivative of (A.37) is written as

$$\dot{V}_{e_{ref}} \leqslant \left[-\lambda_{\min}\left(Q\right) + 2\lambda_{\max}\left(P\right)b_{\max}\left(\left\|\tilde{\theta}\right\| + \dot{\mathcal{K}}_{\max}T\right) + 2 \right] \|e_{ref}\|^2
+ \lambda_{\max}^2\left(P\right)\overline{\omega}_r^2 b_{\max}^2 \left\|\tilde{\theta}\right\|^2 + \lambda_{\max}^2\left(P\right) b_{\max}^2 \overline{\omega}_r^2 \dot{\mathcal{K}}_{\max}^2 T^2 - 2a_0^2 e^{-\frac{\gamma_1}{2}\left(t - t_0^+ - T_s\right)}.$$
(A.38)

As for all $t \ge t_0^+ + T_s$ the parametric error $\tilde{\theta}(t)$ meets the inequality (A.36), then, considering

$$\begin{split} \left\| \tilde{\theta} \left(t \right) \right\|^{2} &\leqslant \left(\beta_{\max} + \frac{2w_{1\max}}{\Omega_{LB}} \right)^{2} e^{-\gamma_{1} \left(t - t_{0}^{+} - T_{0} \right)} + \left(\frac{\gamma_{1} w_{2\max} \left(T \right)}{\Omega_{LB}} \right)^{2} \\ &+ 2 \left(\beta_{\max} + \frac{2w_{1\max}}{\Omega_{LB}} \right) \frac{\gamma_{1} w_{2\max} \left(T \right)}{\Omega_{LB}} e^{-\frac{\gamma_{1}}{2} \left(t - t_{0}^{+} - T_{0} \right)} \\ &\leqslant \left(\beta_{\max} + \frac{2w_{1\max}}{\Omega_{LB}} \right) \left(\beta_{\max} + \frac{2 \left(w_{1\max} + \gamma_{1} w_{2\max} \left(T \right) \right)}{\Omega_{LB}} \right) e^{-\frac{\gamma_{1}}{2} \left(t - t_{0}^{+} - T_{0} \right)} + \left(\frac{\gamma_{1} w_{2\max} \left(T \right)}{\Omega_{LB}} \right)^{2} \\ &= \overline{\beta}_{\max} e^{-\frac{\gamma_{1}}{2} \left(t - t_{0}^{+} - T_{0} \right)} + \left(\frac{\gamma_{1} w_{2\max} \left(T \right)}{\Omega_{LB}} \right)^{2} \end{split}$$

the upper bound of (A.38) is written as follows:

$$\dot{V}_{e_{ref}} \leqslant \left[-\lambda_{\min}\left(Q\right) + 2 + 2\lambda_{\max}\left(P\right)b_{\max} \times \left(\left(\beta_{\max} + \frac{2w_{1\max}}{\Omega_{LB}} \right) e^{-\frac{\gamma_{1}}{2}\left(t - t_{0}^{+} - T_{s}\right)} + \frac{\gamma_{1}w_{2\max}\left(T\right)}{\Omega_{LB}} + \dot{\mathcal{K}}_{\max}T \right) \right] \|e_{ref}\|^{2} + \lambda_{\max}^{2}\left(P\right)\overline{\omega}_{r}^{2}b_{\max}^{2}\overline{\beta}_{\max}e^{-\frac{\gamma_{1}}{2}\left(t - t_{0}^{+} - T_{s}\right)} + \lambda_{\max}^{2}\left(P\right)\overline{\omega}_{r}^{2}b_{\max}^{2}\left(\frac{\gamma_{1}w_{2\max}\left(T\right)}{\Omega_{LB}}\right)^{2} + \lambda_{\max}^{2}\left(P\right)\overline{\omega}_{r}^{2}b_{\max}^{2}\dot{\mathcal{K}}_{\max}^{2}T^{2} - 2a_{0}^{2}e^{-\frac{\gamma_{1}}{2}\left(t - t_{0}^{+} - T_{s}\right)}.$$
(A.39)

There definitely exists a time instant $t_{e_{ref}} \ge t_0^+ + T_s$ and constants $T \to 0$, $a_0 > \lambda_{\max}(P)\overline{\omega}_r b_{\max}\overline{\beta}_{\max}^{\frac{1}{2}}$ such that for all $t \ge t_{e_{ref}}$ it holds that

$$-\lambda_{\min}(Q) + 2 + 2\lambda_{\max}(P) b_{\max}\left(\left(\beta_{\max} + \frac{2w_{1\max}}{\Omega_{LB}}\right) e^{-\frac{\gamma_1}{2}\left(t_{e_{ref}} - t_0^+ - T_s\right)} + \frac{\gamma_1 w_{2\max}(T)}{\Omega_{LB}} + \dot{\mathcal{K}}_{\max}T\right) = -c_1 < 0, \qquad (A.40)$$
$$\lambda_{\max}^2(P) \overline{\omega}_r^2 b_{\max}^2 \overline{\beta}_{\max} - 2a_0^2 = -c_2 < 0.$$

Then the upper bound for the derivative (A.39) for all $t \ge t_{e_{ref}}$ is obtained as

$$\dot{V}_{e_{ref}} \leqslant -\eta_{\overline{e}_{ref}} V_{e_{ref}} + \lambda_{\max}^2(P) \,\overline{\omega}_r^2 b_{\max}^2 \left(\frac{\gamma_1 w_{2\max}\left(T\right)}{\Omega_{LB}}\right)^2 + \lambda_{\max}^2\left(P\right) \overline{\omega}_r^2 b_{\max}^2 \dot{\mathcal{K}}_{\max}^2 T^2, \qquad (A.41)$$

where $\eta_{\overline{e}_{ref}} = \min\left\{\frac{c_1}{\lambda_{\max}(P)}, \frac{c_2\gamma_1}{4a_0^2}\right\}$.

The solution of the differential inequality (A.41) for all $t \ge t_{e_{ref}}$ is written as

$$V_{e_{ref}}(t) \leqslant e^{-\eta_{\overline{e}_{ref}}(t-t_{e_{ref}})} V_{e_{ref}}\left(t_{e_{ref}}\right) + \frac{1}{\eta_{\overline{e}_{ref}}} \left(\lambda_{\max}^{2}\left(P\right)\overline{\omega}_{r}^{2}b_{\max}^{2}\left(\frac{\gamma_{1}w_{2\max}\left(T\right)}{\Omega_{LB}}\right)^{2} + \lambda_{\max}^{2}\left(P\right)b_{\max}^{2}\overline{\omega}_{r}^{2}\dot{\mathcal{K}}_{\max}^{2}T^{2}\right),$$
(A.42)

which completes the proof of statement (ii) of theorem.

Step 3. Owing to (A.36) and (A.42), the error $\tilde{\theta}(t)$ is bounded for all $t \ge t_0^+ + T_s$, and the error $e_{ref}(t)$ — for all $t \ge t_{e_{ref}}$. Then, to prove the statement (i), we need to show that $\tilde{\theta}(t)$ is bounded over $[t_0^+, t_0^+ + T_s]$, and $e_{ref}(t)$ is bounded over $[t_0^+, t_{e_{ref}}^+)$.

In the conservative case, the inequality $\Omega(t) \leq \Omega_{LB}$ is satisfied over $\left[t_0^+, t_0^+ + T_s\right)$, whence, owing to $\dot{\tilde{\theta}}(t) = 0_{n+1}$, if Assumption 1 is met, it follows that the parametric error $\tilde{\theta}(t) = \hat{\theta}\left(t_0^+\right) - \hat{\theta}(t)$ is bounded over $\left[t_0^+, t_0^+ + T_s\right)$ and, as a consequence, for all $t \geq t_0^+$.

Considering the time range $[t_0^+, t_{e_{ref}}]$ and taking into account the notation from (A.3), (A.18), the error equation (3.1) is written in the following form:

$$\dot{e}_{ref}(t) = \left(A_{ref} + e_n b\left(t\right) \left(\hat{\theta}_x\left(t\right) - k_x\left(t\right)\right)\right) e_{ref}\left(t\right) + e_n b\left(t\right) \left(\hat{\theta}^{\mathrm{T}}\left(t\right) - \mathcal{K}^{\mathrm{T}}\left(t\right)\right) \omega_r\left(t\right),$$

which, as it has been proved that $\tilde{\theta}(t)$ is bounded for all $t \ge t_0^+$ and Assumptions 1 and 2 are met, allows one, using Theorem 3.2 from [20], to make the conclusion that 1) $e_{ref}(t)$ is bounded over $[t_0^+, t_{e_{ref}}), 2) \xi(t) \in L_{\infty}$ for all $t \ge t_0^+$.

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TOPICAL ISSUE

Investigation of Feasible and Marginal Operating Regimes of Electric Power Systems

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Abstract—The paper is devoted to the analysis of the feasibility domain of electric power systems. The problems of calculating feasible and marginal regimes of power systems, analyzing the geometry of the feasibility domain, and generating samples in this region are considered. Parallels are drawn with the works of B.T. Polyak on the analysis of the image of a quadratic map, modification of the Newton method and the development of methods for generating asymptotically uniform samples in areas with complex geometry. Particular attention is paid to Newton's method with the transversality condition (TENR), its application for constructing a boundary oracle procedure and utilization for generating samples in the power system feasibility domain.

Keywords: admissible domain of power systems, power flow equations, quadratic mapping image, Newton's method, sampling

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1. INTRODUCTION

The development of theory, models and methods for calculating optimal and marginal operating regimes of the power system remains a challenging and relevant research topic due to the widespread distribution of distributed renewable energy sources, changing patterns of electrical energy consumption and digital transformation in the energy sector. Control of modern power systems requires fast and reliable methods for estimating static stability margins, which are characterized by the distance to the boundary of the feasibility domain. In addition, the growing integration of distributed renewable energy sources is prompting a reassessment of the criteria for optimal grid operating regimes, which shifts frequently operated regimes closer to the boundary. The concept of a feasibility domain for electric power system — a region in the multidimensional space of nodal power injections (the right-hand side of power flow equations) such that this system of equations has at least one real solution — bridges between various problems in energy sector.

Further in the introduction, we discuss the links between the analysis of feasible and marginal operating regimes of a power system with the image of a quadratic mapping, *D*-partition, Newton's method and its modifications, as well as methods for generating asymptotically uniform samples in areas with complex geometry.

1.1. Image of Quadratic Mapping

The steady-state operation regimes are described by power flow equations, reflecting fundamental Ohm's and Kirchhoff's laws they provide the relation between complex voltages and power at the nodes of power system (1)–(2). These equations are quadratic with respect to variable V. In papers [1, 2] B.T. Polyak proposed sufficient conditions for convexity of the image of quadratic



Fig. 1. Convex region of feasible regimes from [4].



Fig. 2. Non-convex region of feasible regimes from [5].

mapping $f : \mathbb{R}^n \to \mathbb{R}^m$ at m = 2, 3, later in [3] a randomized approach for certifying convexity/nonconvexity of the image of quadratic mapping was proposed.

Indeed, feasibility domain of power system has a pretty complicated geometry. Moreover, this complexity holds regardless the number of nodes, one may observe complicated structure for the systems of 3–5 nodes ("nodes" are typical called "buses" in power systems analysis). In 1 presents the cross-section of the feasibility domain for 3 bus system. The area is convex, though it's demonstrated in [4] that it looses convexity for perturbed right-had side of power flow equation.

Examples of more exotic feasibility domains can be found in [5], one of cross-sections of this type for 5-bus system is presented in Fig. 2.

Looking at Figs. 1–2, it is straightforward to recognize a complex internal structure of the feasibility domain. Due to the nonlinearity of the system of power flow equations there are internal bifurcation curves, such that crossing them corresponds to either a change in the number of solutions or the disappearance of solutions, and therefore the admissible state of the system. These

GRYAZINA, BALUEV

equations can have multiple isolated solutions, representing either a stable or unstable equilibrium of a dynamic power system model. The presence of multiple solutions was previously ignored by researchers; their efforts were mainly focused on identifying only one real solution rather than on all isolated solutions. The work [6] is apparently the first to study the phenomenon of multiplicity of solutions to the control system and propose a method for constructing all critical points of the region of admissible modes. Critical points are understood as points of bifurcation curves, the intersection of which changes the number of solutions to the system of power flow equations. Such an analysis of the feasibility domain has much in common with *D*-decomposition method developed in the works of B.T. Polyak [7, 8]. For linear dynamical system *D*-decomposition curve splits the parameter space into regions with different numbers of stable roots of characteristic polynomial, while bifurcation curve (or surface in higher dimensional spaces) separates the regions wit different number of solutions to the power flow equations in thee feasibility domain.

1.2. The Role of Newton Method

Traditionally, Newton–Raphson method is applied for calculating steady state regimes. The introduction of additional variables characterizing stability margins makes the system underdetermined. In this case, the problem of calculating regimes appears in the context of B.T. Polyak's papers [9, 10].

One of the most promising methods for fast calculations of marginal regimes is Newton's method with the transversality condition (TENR, Transversality Enforced Newton–Raphson) [11], where, in addition to an additional variables, the condition of degeneracy of the Jacobian matrix is added.

The TENR method is conceptually similar to, but mathematically different from, traditional methods based on the standard Newton method. In TENR, the standard system of power flow equations is complemented by the transversality condition. This constraint regularizes the initially degenerate system at the marginal point and ensures the convergence of Newton's method. In addition, TENR allows the steady state calculation to take into account any technical constraints, which can be represented either as equalities or inequalities. From a computational point of view, a key advantage of TENR is its simple form of writing transversality conditions, which does not require explicit tracking and initialization of zero eigenvectors of the Jacobian. This simplification results in a smaller system of nonlinear equations and also allows for easier initialization of the algorithm.

The TENR method has a number of advantages: the algorithm is numerically stable in the immediate vicinity of the boundary, as well as at the feasibility boundary; it weakly depends on the starting point; decomposition of the Jacobian matrix by singular values has been implemented, which allows us to analyze the sensitivity of the power system and identify the most "effective nodes" for applying control actions. Based on TENR, it is possible to solve the problem of estimating the transfer capability margins [12], as well as online assessment of voltage stability margins [13]. The method has been tested on a number of IEEE benchmark systems as well as on a model of the power system of the Russian Far East [14].

1.3. Sampling in Feasibility Domain

Knowledge about the feasibility domain geometry of power system and its boundaries allows us to make fast estimation of the stability margins and to calculate optimal emergency control actions. The challenge of ensuring reliable and secure real-time operation of power systems is increasing as the current operating regime rapidly changes due to uncertainties associated with increased renewable generation, less predictable demand and various unexpected circumstances. Therefore, to avoid any undesirable system behavior or large-scale power outage, real-time evaluation of voltage stability margins is required. Such an assessment is a challenging task that requires significant computational resources, mainly due to the constantly changing state of operation. Both during the planning and operational stage, safe operation of the network requires voltage stability, which is the ability of the power system to maintain acceptable voltage levels on all buses after exposure to disturbances [15].

Modern power systems are more vulnerable in terms of stability because they operate close to the boundary of the feasibility region. Voltage instability occurs in electrical networks when the operating mode approaches the point of collapse or the point of saddle-node bifurcation, after which the real solution to the steady-state equations vanishes or the number of solutions to the system of steady-state equations changes. You can clarify your description of the feasibility domain via sampling, i.e. generating parameters of feasible modes. Such parameter sets are also useful for tuning machine learning algorithms. One of the directions of B.T. Polyak's research was the development of methods for generating asymptotically uniformly distributed samples in complex domains [16, 17].

This paper provides a detailed description of the TENR method as the most effective tool for calculating the marginal states of a power system, and also shows how to use TENR to build a boundary oracle procedure to generate samples in the feasibility domain.

The paper is organized as follows: Section 2 presents the problem formulation. Section 3 describes the TENR method and discusses the strategy for choosing the optimal step size for its implementation. Section 4 is devoted to the problem of generating samples in the feasibility domain of power system. Section 5 provides numerical examples illustrating the effectiveness of the TENR method both for calculating marginal regimes (boundary points of the feasibility domain) and for generating samples.

2. PROBLEM STATEMENT

Power system marginal states (marginal operating regimes) assessment is closely related to the power flow analysis (so-called regime). A regime is a state of the power system that can be characterized by quantitative indicators: power, voltage, current, phase angles of the EMF vectors, and others. A regime can be categorized as transient or steady-state, depending on the rate of their change. A steady-state is one in which the parameters remain constant over the considered time interval or change relatively slowly [18]. Since a regime has quantitative characteristics, it can be calculated and evaluated. The calculation of the steady-state regime (power flow analysis) involves determining all parameters of the steady-state regime given the known system parameters (circuit diagrams, line impedance, etc.) and some specified regime parameters [19]. The set of equations based on the equivalent circuits of the power system, as well as Ohm's and Kirchhoff's laws, constitutes the mathematical model of the steady-state regimes of power systems.

In the theory of electrical systems, there are numerous available mathematical models, each with its advantages and disadvantages. In this work, the model used is the system of power balance equations presented in a rectangular form. The voltage is represented as a complex: $\hat{V}_i = V_i^r + jV_i^m \in \mathbb{C}$. G_{ij} and B_{ij} are the real and imaginary parts of the complex admittance $\hat{Y}_{ij} = G_{ij} + jB_{ij} \in \mathbb{C}$. The system consists of n buses, where $\mathcal{N} = \{1, 2, \ldots, n\}$ is the set of buses excluding the balancing (slack) bus \mathcal{S} ; the set of PQ buses (load buses) is denoted as \mathcal{L} ; and the set of PV buses (generator buses) is denoted as \mathcal{G} . For each $i \in \mathcal{N}$, the values of the nodal active power injections can be computed as follows [18, 20, 21]:

$$\sum_{k=1}^{n} \left\{ V_i^r (G_{ik} V_k^r - B_{ik} V_k^m) + V_i^m (G_{ik} V_k^m + B_{ik} V_k^r) \right\} = P_i(x) - \lambda (P_{\text{gen},i} - P_{\text{load},i}),$$
(1)

where the vector $\mathbf{x} \in \mathbb{R}^n$ is a set of variables (the magnitude of voltages and phase angles at the buses for each bus in the system). Similarly, for each $i \in \mathcal{L}$, one can write the equation for the

nodal reactive power injections:

$$\sum_{k=1}^{n} \left\{ V_i^m (G_{ik} V_k^r - B_{ik} V_k^m) - V_i^r (G_{ik} V_k^m + B_{ik} V_k^r) \right\} = Q_i(x) - \lambda (Q_{\text{gen},i} - Q_{\text{load},i}).$$
(2)

Subscripts "gen" and "load" denote the levels of generation and load at the buses, respectively. The parameter λ is a coefficient used to "stress" the system, meaning that loads are gradually increased. When $\lambda = \lambda_{\text{max}}$, the system reaches its marginal state. Unlike the representation in polar coordinates, the formulation in Cartesian coordinates requires an additional set of equations to account for the voltage limitations at the PV buses. Thus, for each $i \in \mathcal{G}$,

$$(V_i^r)^2 + (V_i^m)^2 - |\hat{V}_i|_{\text{ref}}^2 = 0,$$
(3)

where $|V_i|_{\text{ref}}$ is the reference voltage magnitude at the specific bus.

The standard system of power flow equations can be generally expressed as follows:

$$\mathcal{F}(x,\lambda) = 0,\tag{4}$$

where \mathcal{F} represents k nonlinear equations, including both power balance equations (such as in (1) and (2)) and various technological constraints presented as equalities. The parameter λ is the loading coefficient that characterizes the system's proximity to the steady-state equation solvability boundary.

The finding of marginal states means to find such λ_{\max} that the solution of the system (4) exists for all $0 \leq \lambda \leq \lambda_{\max}$ but do not exist when $\lambda > \lambda_{\max}$.

From a mathematical perspective, finding of marginal states involves solving the system of equations (4) under the condition that the Jacobian matrix is singular:

$$g(x) = \det \nabla_x \mathcal{F}(x, \lambda) = 0.$$
(5)

It follows that, to find the marginal state (stability boundary), it is necessary to solve the system of equations (4) together with the additional condition that accounts for the singularity of the Jacobian matrix (5).

3. TRANSVERSALITY ENFORCED NEWTON-RAPHSON METHOD

To solve the system of power flow equations, numerical iterative methods must be employed, which improve the approximation of the initial variables with each iteration. One of the most common and accessible methods is the Newton–Raphson method.

It should be noted that the classical Newton–Raphson method has several drawbacks, including convergence dependence on the chosen initial conditions and poor convergence in close proximity to the stability boundary. The reason for this is the poor conditioning of the Jacobian matrix. Therefore, the standard Newton method provides a consistently underestimated assessment of the power system's stability margin. If the numerical method remains stable at the feasibility boundary, the distance to the marginal state can be determined more accurately.

There is a method that addresses these issues — the TENR method.

During the marginal state analysis, when λ reaches its maximum value λ_{\max} , the Jacobian matrix of the power flow system becomes singular. Under these circumstances, the Newton method's computational step $J^{-1}\mathcal{F}(x)$ increases, keeping the classical method numerically unstable. As a result, the method may fail to converge or require too many iterations to achieve a result. In the TENR method, an additional condition that accounts for the Jacobian matrix's singularity at the feasibility boundary is added to the base system of equations, with λ also treated as a variable. Thus, the solution domains of the original and the augmented systems of equations coincide. Within the TENR method, the condition accounting for the Jacobian's singularity at the stability boundary is called the transversality condition $g(\mathbf{x})$. Numerous possible variations of the condition $g(\mathbf{x})$ are available, as presented in [11]. The least computationally expensive approach is based on singular value decomposition.

In general form, the system of equations for finding the limit modes can be written as follows:

$$\mathcal{F}(x,\lambda) = 0,$$

$$g(x) = 0$$
 (6)

The system (6) can be numerically solved using the standard Newton method. Undertaking a linearization of equation utilizing the first-order Taylor series within the realms of x and λ results in:

$$\begin{bmatrix} \mathcal{F} \\ g \end{bmatrix} + \begin{pmatrix} \nabla_{\mathbf{x}} \mathcal{F} & \nabla_{\lambda} \mathcal{F} \\ (\nabla_{\mathbf{x}} g)^{\top} & 0 \end{pmatrix} \begin{bmatrix} \Delta x \\ \Delta \lambda \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}.$$
 (7)

In the TENR method, the so-called extended Jacobian matrix $\mathcal{J}(x,\lambda)$ is used in the calculations:

$$\mathcal{J}(x,\lambda) = \begin{pmatrix} \nabla_x \mathcal{F} & \nabla_\lambda \mathcal{F} \\ (\nabla_{\mathbf{x}} g)^\top & 0 \end{pmatrix}.$$
 (8)

The increments of the unknowns Δx and $\Delta \lambda$ are determined as follows:

$$\begin{bmatrix} \Delta x \\ \Delta \lambda \end{bmatrix} = - \begin{pmatrix} \nabla_{\mathbf{x}} \mathcal{F} & \nabla_{\lambda} \mathcal{F} \\ (\nabla_{\mathbf{x}} g)^{\top} & 0 \end{pmatrix}^{-1} \begin{bmatrix} \mathcal{F} \\ g \end{bmatrix}.$$
(9)

Using the calculated increments of the variables, the values of the variables at the next step are determined as follows:

$$\mathcal{N}(x,\lambda) := \begin{bmatrix} x\\ \lambda \end{bmatrix} - \alpha \begin{bmatrix} \begin{pmatrix} \nabla_x \mathcal{F} & \nabla_\lambda \mathcal{F} \\ (\nabla_x g)^\top & 0 \end{bmatrix}^{-1} \begin{bmatrix} \mathcal{F} \\ g \end{bmatrix} \end{bmatrix}.$$
 (10)

The parameter α determines the step size in the Newton method, which must be chosen to be sufficiently small. The calculation is performed iteratively until the established convergence criterion is reached:

$$\|\mathcal{N}^{(\kappa)}(x,\lambda) - \mathcal{N}^{(\kappa-1)}(x,\lambda)\| \leqslant \epsilon, \quad \kappa = 1, 2, \dots,$$
(11)

where κ is the iteration counter and ϵ is the desired calculation accuracy.

Newton-Raphson method has quadratic convergence if the initial design point is chosen in close proximity to the actual solution. However, the Newton-Raphson method may diverge. To prevent such situations, it is necessary to optimally select the Newton iteration step size. The methodology for choosing the optimal step size is presented below.

3.1. Optimal Step-Size Strategy

The Newton-Raphson method is highly sensitive to the initial approximation. In some cases, an improper choice of the initial guess can lead to a large number of iterations or the method may fail to converge altogether. To ensure faster convergence and global convergence with any reasonable initial approximation, the system of equations should be supplemented with a damping coefficient α , as introduced in (10). One of the most efficient and computationally simple methods is to adjust α at each iteration.



Fig.3. Optimal step size $\alpha^{(\kappa)}$ selection for each iteration of the TENR method for IEEE test systems.

The original system of equations can be written in a compact form as:

$$\mathcal{H}(z) = \begin{cases} \mathcal{F}(x,\lambda) &= 0\\ g(x) &= 0. \end{cases}$$
(12)

The vector z represents the set of variables $z = [x, \lambda]^{\top}$. In the Cartesian formulation, the equations considered in (4) are a set of quadratic equations, while the transversality condition g(x) = 0 is a linear equation, especially when the transversality condition is expressed through the singular value decomposition of the Jacobian. Therefore, for the point $z^{(\kappa)}$ and the vector $\Delta z^{(\kappa)}$, the system (12) can be approximated by a second-order Taylor expansion as

$$\mathcal{H}(z^{(\kappa)} + \Delta z^{(\kappa)}) \approx \mathcal{H}(z^{(\kappa)}) + \left[\nabla_z \mathcal{H}(z^{(\kappa)})\right] \Delta z^{(\kappa)} + \frac{1}{2} (\Delta z^{(\kappa)})^\top \left[\nabla_{zz} \mathcal{H}(z^{(\kappa)})\right] \Delta z^{(\kappa)}.$$
 (13)

Since all the equations in (4) are quadratic, and g(x) is linear, (13) holds exactly. The optimal step size $\alpha^{(\kappa)}$ in the direction of the vector $\Delta z^{(\kappa)}$ is found by solving the following minimization problem:

$$\mathcal{H}(\alpha) = \left\{ \mathcal{H}(z^{(\kappa)}) + \alpha [\nabla_z \mathcal{H}(z^{\kappa})] \ \Delta z^{(\kappa)} + \frac{\alpha^2}{2} (\Delta z^{(\kappa)})^\top [\nabla_{zz} \mathcal{H}(z^{(\kappa)})] \ \Delta z^{(\kappa)} \right\},\tag{14}$$

$$\alpha^{(\kappa)} = \underset{\alpha}{\operatorname{argmin}} \ \frac{1}{2} \|\mathcal{H}(\alpha)\|_2^2.$$
(15)

The optimization problem (15) can be solved explicitly by applying the first-order optimality condition.

Figure 3 shows the values of $\alpha^{(\kappa)}$ at each iteration of the TENR method for the IEEE test systems consisting of 14, 30, 118, and 300 buses. These test cases include the standard problem of determining the marginal state under initial conditions, where all bus voltage magnitudes are 1, and the corresponding angles are 0. It can be observed that the initially proposed step size strategy leads to small values of α . However, as the algorithm approaches the solution, the step size gradually increases. This behaviour can be explained by the fact that, in the initial iterations, the first-

order Taylor approximation of the equations in (12) poorly satisfies the equality. As the algorithm progresses, this approximation becomes more accurate, leading to an increase in the step size α .

4. SAMPLING PARAMETERS OF FEASIBLE REGIMES

For regions with complicated geometry (non-convex, represented by nonlinear equations), which certainly includes the region of feasible power system modes, a working method for obtaining asymptotically uniform samples is based on the use of a version of the Monte Carlo method, namely Markov Chain Monte Carlo (MCMC) [22]. One of the most famous and effective MCMC-type algorithm is called Hit-and-Run (HR), originally proposed in [23], and later rediscovered and analyzed in detail in [24]. Unfortunately, even for simple ill-posed domains (for example, level sets of ill-conditioned functions), the HR method does not work, or at least is computationally inefficient [25].

The variety of applications as well as drawbacks of existing random walk methods open up wide scope for improvement of random walk algorithms. In particular, in the works of B.T. Polyak, it was presented an attempt to use barrier functions (well known in the analysis of interior point methods for convex optimization) and combine them with random walks based on Markov chains. As a result the Barrier Monte Carlo method [26] was proposed, whose mixing properties in some cases turned out to be preferable to the HR method. However, the complexity of each iteration remained quite high (in particular, at each iteration it is required to calculate $(\nabla^2 F(x))^{-1/2}$, where F(x) is the barrier function for the region Q). Moreover, this approach cannot accelerate the convergence of the distribution of the resulting points to a uniform one for areas similar to simplexes. Finally, in [27] the idea of Billiard Walk was presented, and theorems on the asymptotic uniformity of generated samples have been proved for the convex and non-convex cases. In contrast to the Ball Walk method, where each subsequent point is selected uniformly random at the intersection of the ball centered at the current point and the region under consideration, and the Hit-and-Run method, where the next point is randomly selected uniformly on a random chord drawn through the current point, the Billiard Walk method is based on a billiard trajectory of random length, released from the current point in a random direction.

The Hit-and-Run method and its improved modification, the Billiard Walk method, provide a useful tool for generating samples in the feasibility domain. The only requirement for a domain is that it must have a boundary oracle procedure and, in the case of a Billiard Walk, a way to recover the normal to the boundary.

Let us describe the application of the Hit-and-Run method and the boundary oracle procedure necessary for its implementation for the power system feasibility domain. The generated samples are located in the multidimensional space of nodal power injections $S_i = P_i + jQ_i$, i = 1, ..., n, which includes active power P_i and reactive power Q_i .

- 1. Choose initial regime S^0 , k = 0. It can be arbitrary feasible point or so-called flat start: $V_i = 1$, $P_i = 0, Q_i = 0; i = 1, ..., n$.
- 2. Generate random direction d^k , which is uniform random on the unit sphere in \mathbb{R}^{2n} . Components of d correspond to increments of active and reactive powers in the righ-had side of the equations (1)-(2).
- 3. Calculate marginal states in the directions d^k and $-d^k$ as well as corresponding $\overline{\lambda}$, $\underline{\lambda}$ via TENR method.
- 4. Update k = k + 1 and specify the next sample as $S^k = S^{k-1} + td$, where scalar t is uniform random in $[-\underline{\lambda}, \overline{\lambda}]$.
- 5. Save S^k and corresponding regime parameters. Go to Step 2.

For implementation of Billiard Walk algorithm eigenvector corresponding to zero eigenvalue of the Jacobian should be used as a normal to the boundary.

GRYAZINA, BALUEV

5. NUMERICAL EXPERIMENTS

Let's illustrate the effectiveness of the TENR method and its modifications for stability margin assessment and generating samples in the power system feasibility domain. Several power systems models from the IEEE collection [28, 29], widely used in academic research, were chosen as examples. The TENR method is integrated into the open-source software package PESOL [30].

5.1. Determination of Marginal States

The accuracy comparison of stability margin assessment was conducted between TENR and three of the most common limit state estimation methods integrated into various software packages: Continuation Power Flow (CPF), Power System Analysis Toolbox (PSAT), and MATPOWER. The comparison results of the λ values, characterizing the stability margins, are presented in Table.

with analogues (without taking into account voltage constraints)				
IEEE-scheme	λ_{TENR}	λ_{CPF}	λ_{PSAT}	λ_{MAT}
9 buses	1.486	1.486	1.481	1.483
14 buses	3.061	3.061	3.059	3.056
30 buses	1.958	1.957	1.959	1.838
57 buses	0.893	0.892	0.891	0.890
118 buses	2.188	2.187	2.187	2.184
300 buses	0.430	0.430	0.429	0.425

Comparison of the stability margin obtained using the TENR method with analogues (without taking into account voltage constraints)

The comparison results between the TENR method and its direct competitors show that the stability margin calculated using TENR is not lower than the values obtained using other methods in all considered cases. For some cases, TENR indicated a slightly higher actual stability margin than other methods. The main advantage of TENR is the calculation speed and scalability (calculation of power systems with thousands of buses). A detailed comparison of the calculation speed of TENR with its direct competitors is presented in [14].

5.2. Generation of Parameters for Marginal States

In this work, a five-bus scheme, shown in Fig. 4, is considered as an example. This system is a modified example first presented in [31]: Bus 1 is the slack bus with voltage $\hat{V}_1 = 1.0$. The adopted description in power engineering of complex voltage in polar form $|V|e^{j\delta}$ is used here, where the



Fig. 4. 5-bus power system test case.



Fig. 5. Cross-section of the feasible region by P_2-P_3 parameter plane with a fixed value $Q_3 = 2 p.u.$ (80 feasible points).



Fig. 6. Cross-section of the feasible region by P_2-P_3 parameter plane with a fixed value $Q_3 = 2 p.u.$ (200 feasible points).

GRYAZINA, BALUEV

phase angle is presented following the magnitude in the form $V \angle \delta$. The other buses in the system are PV buses with a fixed voltage value of 1.0 (p.u.), except for Bus 3, which is a PQ bus with a complex voltage value of $\hat{V}_3 = |V_3|e^{j\delta_3}$. It is also assumed that synchronous compensators with zero active power are installed at Buses 4 and 5. Consequently, the solution space is limited to the parameters P_2, P_3, Q_3 .

Consider a cross-section of the feasibility region by the P_2-P_3 parameter plane, with the remaining parameters of the right-hand side of the power flow equations fixed as indicated above, $Q_3 = 2$. The results of generating 80 and 200 feasible regimes are shown in Figs. 5 and 6. The dots correspond to the internal points of the feasible operating region, while the crosses represent the limit operating regimes. The figures show that 200 generated feasible operating modes are sufficient for solving practical optimization problems, and the limit modes fairly densely cover the boundary of the permissible region.

6. CONSLUSION

This paper describes the main difficulties encountered in calculating the parameters of critical regimes in power systems and presents the TENR method, which currently appears to be the most effective method for marginal state assessment. Moreover, for the first time, the use of the TENR method for constructing a boundary oracle procedure and generating points within the feasible operating region has been presented and tested.

Surprisingly, the tasks of analyzing feasible and marginal states in power systems draw their solutions from the works of B.T. Polyak. His results on the convexity of the image of quadratic mappings, modifications of the Newton method, and detailed descriptions of random walk schemes for generating points in regions with complex geometry have proven extremely useful for power engineering. The authors do not doubt that researchers will discover many more such connections and bridges in the future.

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TOPICAL ISSUE

Iterative Methods with Self-Learning for Solving Nonlinear Equations

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Abstract—This paper is devoted to the problem of solving a system of nonlinear equations with an arbitrary but continuous vector function on the left-hand side. By assumption, the values of its components are the only a priori information available about this function. An approximate solution of the system is determined using some iterative method with parameters, and the qualitative properties of the method are assessed in terms of a quadratic residual functional. We propose a self-learning (reinforcement) procedure based on auxiliary Monte Carlo (MC) experiments, an exponential utility function, and a payoff function that implements Bellman's optimality principle. A theorem on the strict monotonic decrease of the residual functional is proven.

Keywords: nonlinear equation, iterative methods, reinforcement, Monte Carlo experiment

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1. INTRODUCTION

The vast majority of applied problems lead to the need to solve nonlinear equations. Parameterized iterative methods are a classical tool yielding approximate solutions of nonlinear equations under definite conditions [1–4]. These conditions are certain properties of the functions (convexity, concavity, differentiability, etc.) included in the equations and interval *sufficient* parametric conditions ensuring the convergence of the corresponding iterative method.

The increasing complexity of functions narrows the set of their classes where such properties can be verified and the verification results can be used in suitable iterative methods. On the other hand, interval conditions on the parameters of iterative methods significantly depend on the properties of functions that are generally unverifiable.

To find a way out of this situation, the ideas of reinforcement learning can be applied to the iterative computational process to determine the values of its parameters using statistical Monte Carlo (MC) experiments and a game-theoretic mathematical model [5, 6]. The essence of this branch of machine learning is to train an object (model, algorithm, etc.) by interacting not with a "teacher" (supervised learning) but with an "environment," using the trial-and-error method, followed by rewards or penalties for its results.

This approach was employed in clustering and recognition problems, apparently because of the ability to calculate the so-called feature characteristics in the form of "distances" between objects. The distance matrix was adopted to arrange some "rewards" or "penalties" when tuning the algorithm parameters. The algorithms considered were neural networks [7] and game-theoretic models implementing the principle of competition between neural network nodes [8]. In particular, the advantage was given to the nodes with the minimum distance between objects at each step of the algorithm.

Subsequently, reinforcement learning based on the automata models of interaction between an object (agent) and an environment was simulated in game-theoretic terms (strategies, utility functions, and payoffs) and was actively developed [9]. Many algorithms appeared, differing in the models and amounts of a priori information about the environment, algorithms for choosing strategies, and procedures for designing utility functions [10–13].

An important component of reinforcement learning procedures is MC experiments intended to simulate agent's strategies [14]. They are used to average a fixed number of current rewards with their discounting. The resulting function depends on the state of the environment and the agent's strategy; it is taken as a utility function (an analog of the objective function in supervised learning procedures) and is sequentially maximized during the learning process [15, 16] using Bellman's optimality principle [17] in combination with stochastic approximation [18].

This paper considers the problem of numerically solving a system of nonlinear equations using a parameterized iterative procedure whose convergence depends on the parameter values. To determine these values, we develop a reinforcement learning procedure based on a game-theoretic model.

The problem addressed below was actively discussed and shaped under the influence of Boris Polyak. The author was fortunate to work and be friends with him for many years. The blessed memory of Boris will always be the author's compass in life.

2. PROBLEM STATEMENT

Consider the nonlinear equation

$$\mathbf{f}(\mathbf{x}) = \mathbf{1}, \quad (\mathbf{f}, \mathbf{x}, \mathbf{1}) \in \mathbb{R}^n.$$
(1)

By assumption, the only a priori information available about the function **f** is the values of its components $f_i(\mathbf{x}^{(k)}), i = \overline{1, n}; k = 1, \dots$

We introduce the residual functional

$$J(\mathbf{x}) = \|\mathbf{f}(\mathbf{x}) - \mathbf{1}\|^2 \ge 0.$$
⁽²⁾

The absolute minimum of this functional is zero. In the general case, it is not unique, i.e., there exists a finite set $\mathbb{X} = \{\mathbf{x}_*^{(1)}, \dots, \mathbf{x}_*^{(r)}\}$ of points at which the residual functional vanishes. In this situation, any solution from the set \mathbb{X} will be considered suitable.

An approximate solution of this equation is determined using an iterative Markov-type procedure. In this procedure, the approximate solution $\mathbf{x}^{(p+1)}$ at step (p+1) is set equal to the value of the operator $\mathcal{B}[\mathbf{x}^{(p)}, \mathbf{a}^{(p)}]$ of the iterative procedure at step p, depending on the values of the components of the function $\mathbf{f}(\mathbf{x}^{(p)})$ and the parameter vector $\mathbf{a}^{(p)} \in \mathcal{A} \subset \mathbb{R}^r$ that adjusts the qualitative properties of the iterative process:

$$\mathbf{x}^{(p+1)} = \mathcal{B}[\mathbf{f}(\mathbf{x}^{(p)}), \mathbf{a}^{(p)}].$$
(3)

Qualitative properties often include *convergence*, the rate of convergence, and accuracy. The conditions for ensuring these properties are formulated in terms of the vector **a** and interval inequalities depending on the properties of the operator \mathcal{B} and those of the function $\mathbf{f}(\mathbf{x})$.

However, the function $\mathbf{f}(\mathbf{x})$ may have an arbitrary structure, making it impossible to postulate or reveal its properties. As a result, these inequalities become analytically unverifiable.

POPKOV

To find a way out of this situation, we utilize the ideas of *reinforcement*, which are actively used in various implementations in modern machine learning procedures. In this case, reinforcement is intended to determine, at each step of the iterative procedure, a suitable parameter vector **a** via an appropriate self-learning procedure.

We propose a game-theoretic model to calculate the suitable parameters **a** of the iterative procedure (3). This model operates in the intervals between steps p and (p + 1) and simulates the behavior of an *agent*, i.e., a strategy for varying the parameters **a** depending on the response quality of an *environment*. The quality is characterized by a conditional *payoff*, a function that depends on the values of the residual functional and its decrement.

3. STRUCTURE OF THE REINFORCEMENT PROCEDURE

Consider the original problem (1) and find its solution by minimizing the residual functional

$$J(\mathbf{x}) \Rightarrow \min, \quad \mathbf{x} \in \mathbb{R}^n.$$
 (4)

In some applications, it may be useful to transform problem (1). We introduce the new variables

$$z_i = \frac{1}{1 + \exp(-b_i x_i)}, \quad x_i = \frac{1}{b_i} \ln \frac{z_i}{1 - z_i}, \quad i = \overline{1, n}.$$

Then problem (1) takes the form

$$J(\mathbf{z}) = \|\Psi(\mathbf{z})\| \Rightarrow \min, \ \mathbf{z} \in Z_+^n = [\mathbf{0}, \mathbf{1}], \quad \Psi(\mathbf{z}) = \mathbf{f}(\mathbf{z}) - \mathbf{1}.$$

Problem (1) will be solved using the iterative procedure (3) under the assumption that the parameters **a** are of interval type: $\mathbf{a} \in [\mathbf{a}^-, \mathbf{a}^+]$.

To determine the values of the components of the vector **a** in the procedure (3), we employ the *reinforcement* technology, implementing it in the interval between steps p and (p + 1) of the iterative procedure (3).

This technology is based on a game-theoretic model simulating the game of an *agent* with an *environment*. The agent generates *strategies* (actions) that cause changes in the environment. The magnitude of these changes is characterized by a *utility function*. The value of a *payoff function* depends on the success of the agent's strategy and its utility for the environment.

In the interval between the successive steps of the iterative procedure, a statistical simulation is carried out via a given number M of MC experiments that simulate the agent's strategies, i.e., the values of the components of the vector $\mathbf{a}^{(p,k)}$, where $k = \overline{1, M}$.

As the agent's actions, we will consider the vector

$$\mathbf{x}^{(p,k+1)} = \mathcal{B}[\mathbf{f}(\mathbf{x}^{(p,k)}), \mathbf{a}^{(p,k)}], \quad p = \text{fix}, \ k = \overline{1, M}.$$
(5)

In this problem, the environment is the residual functional $J(\mathbf{x} | \mathbf{a})$. The MC-simulated actions of the agent yield a sequence of M residuals,

$$J(\mathbf{x}^{(p,1)} | \mathbf{a}^{(p,1)}), \dots, J(\mathbf{x}^{(p,M)} | \mathbf{a}^{(p,M)}),$$
(6)

and their decrements,

$$u^{(p,k)}(\mathbf{a}^{(p,k)}) = J(\mathbf{x}^{(p,k+1)} | \mathbf{a}^{(p,k)}) - J(\mathbf{x}^{(p,k)} | \mathbf{a}^{(p,k-1)}), \quad k = \overline{1, M}.$$
(7)

We introduce a *utility function* to characterize the response quality of the environment measured by the decrement:

$$\varphi(u^{(p,k)}(\mathbf{a}^{(p,k)})) = \alpha \exp[u^{(p,k)}(\mathbf{a}^{(p,k)})].$$
(8)

The quality of the agent's strategies is assessed in terms of a *payoff function* that characterizes the dependence of the agent's payoff on its strategy. Choosing an appropriate payoff function seems to be a creative task [2] involving some enumeration. Several general properties of this function can be declared. It is a continuous and bounded function of the following form:

$$Q(\mathbf{a}^{(p,k)}) = \begin{cases} l(u^{(p,k)}(\mathbf{a}^{(p,k)})) & \varphi(u^{(p,k)}(\mathbf{a}^{(p,k)})) \leq 1\\ 0 & \varphi(u^{(p,k)}(\mathbf{a}^{(p,k)})) > 1, \end{cases}$$
(9)

with the function

$$l(u^{(p,k)}(\mathbf{a}^{(p,k)})) = \begin{cases} \alpha \,\varphi(u^{(p,k)}(\mathbf{a}^{(p,k)})), & 0 \ge u^{(p,k)}(\mathbf{a}^{(p,k)}) \ge -U, \\ 0, & u^{(p,k)}(\mathbf{a}^{(p,k)}) \ge 0, \end{cases}$$
(10)

where U is the limit of the decrement's magnitude.

MC experiments yield a value set of the payoff functions. Following the concept of reinforcement as applied to the iterative procedure (3), we determine the optimal value of the parameter $\mathbf{a}^{(p+1)}$ by the rule

$$\mathbf{a}^{(p+1)} = \mathbf{a}^{(p)} + \beta \arg \max_{1 \le j \le M} Q(\mathbf{a}^{(p,k_j)}).$$
(11)

If the agent chooses its strategy by the rule (11), in view of (9), we have

$$J(\mathbf{a}^{(p+1)}) < J(\mathbf{a}^{(p)}). \tag{12}$$

Thus, the following result has been established for the properties of the residual sequence in the iterative reinforcement procedure (8)-(11):

Theorem 1. Assume that:

a) The only a priori information available about the function $\mathbf{f}(\mathbf{x})$ in (1) is the values of its components $f_i(\mathbf{x}^{(k)}), i = \overline{1, n}$.

b) The parameters of the iterative procedure **a** are chosen by the rule (12), (11), (9).

Then the iterative procedure (5) with reinforcement (8)–(11) generates a strictly monotonically decreasing sequence of the residual functionals $J(\mathbf{x})$ (4).

This theorem is not a convergence theorem for the iterative procedure in the mathematical sense (convergence to one of the solutions). However, it is known that this solution corresponds to a zero residual value. The theorem states that the sequence of residuals is strictly monotonically decreasing. Since the calculation error is finite and can be specified, the final value of the parameters **a** obtained when reaching this error can be taken as a solution.

4. CONCLUSIONS

This paper has been devoted to the problem of solving a system of nonlinear equations with continuous functions on the left-hand sides. By assumption, the only a priori information available about these functions is their values. To find solutions under such conditions, an iterative procedure with parameters has been used: by tuning their values, it is possible to ensure the convergence of the procedure in some sense.

It has been proposed to employ the ideas of reinforcement, which are being rather actively developed in the theory and practice of machine learning. A self-learning procedure has been designed in which a given number of MC experiments are carried out at each iteration step to simulate the agent's strategy (the values of the parameters of the iterative procedure). In this procedure, the environment is the residual functional (5), and its response to the agent's actions is

the decrement (6). For an acceptable evolution of the iterative process, the decrement magnitude must decrease. The decrement has been characterized by an exponential utility function so that smaller decrement magnitudes correspond to larger values of the utility function. The agent's actions, i.e., the implemented parameters of the iterative procedure, have been assessed in terms of a payoff function whose morphology considers both the state of the environment and the degree of success of the agent's actions.

It has been proven that, due to this self-learning procedure, the iterative reinforcement algorithm generates a strictly monotonically decreasing sequence of residual functionals.

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AUTOMATION AND REMOTE CONTROL Vol. 85 No. 5 2024

548